

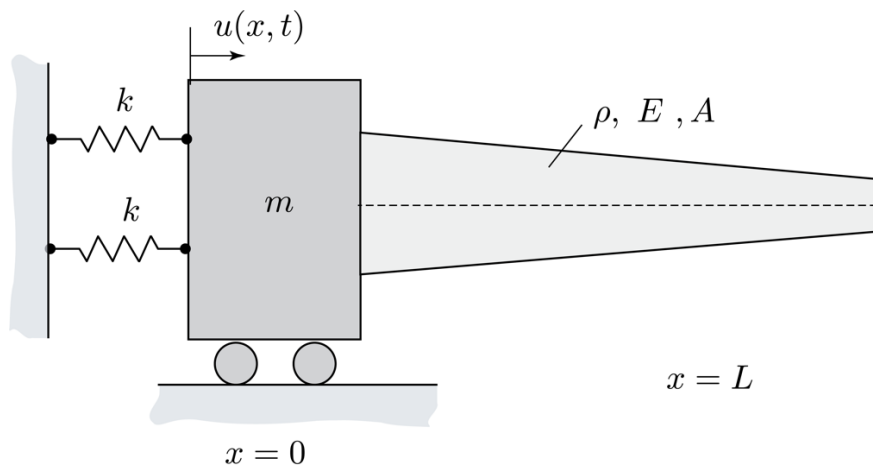
**ME 563 - Fall 2023**  
**Test Problem 1 – 20 points**

Name \_\_\_\_\_

The longitudinal motion of the rod shown below is described by  $u(x,t)$ . The rod has length  $L$ , mass density  $\rho$ , cross sectional area  $A$ . Where the cross sectional varies as

$$A(x) = \left( 2A_o - \frac{A_o}{L}x \right)$$

at  $x=L$  a lumped mass,  $m$ , is attached to beam. Attached to the lumped mass are two springs of stiffness  $k$ .



- State the geometric boundary conditions at  $x=0$ , and derive the natural boundary conditions at  $x=L$ . For the natural boundary conditions an **accurate Freebody diagram must be provided and used in the derivations.**
- Write governing partial differential equation of motion for the system. No FBD diagram is needed answer.
- Assuming a spatiotemporal solution for  $u(x, t) = U(x)T(t)$ , Convert the boundary conditions found in a) to spatial boundary in terms of  $U(x)$  and its associated spatial derivatives. Do not find the characteristic equation.

a)  $\frac{\partial u(L,t)}{\partial x} = 0$



$$\sum F_x = -2k u(L,t) + EA \frac{\partial u(L,t)}{\partial x} = m \frac{\partial^2 u(L,t)}{\partial t^2}$$

$$b) \frac{\partial}{\partial x} \left( EA(x) \frac{\partial u}{\partial x} \right) = \rho A(x) \frac{\partial^2 u}{\partial t^2} \rightarrow \frac{\partial}{\partial x} \left( E(2A_0 - A_0 x/L) \frac{\partial u}{\partial x} \right) = \rho (2A_0 - A_0 x/L) \frac{\partial^2 u}{\partial t^2}$$

$$-EA_0 \frac{\partial u}{L \partial x} + E(2A_0 - A_0 x/L) \frac{\partial^2 u}{\partial x^2} = \rho (A_0 - A_0 x/L) \frac{\partial^2 u}{\partial t^2}$$

$$c) u(x,t) = U(x)T(t)$$

$$\frac{\partial u}{\partial x} = U'(x)T(t)$$

$$\frac{\partial^2 u}{\partial t^2} = -\omega^2 U(x)T(t)$$

$$\frac{\partial u}{\partial x}(0,t) = U'(0)T(t) = 0 \quad U'(0) = 0$$

$$+EA_0 \frac{\partial u(0,t)}{\partial x} - k_{eq} u(0,t) = m \frac{\partial^2 u(0,t)}{\partial t^2}$$

$$+EA U'(0)T(t) - k_{eq} U(0)T(t) = -m\omega^2 U(0)T(t)$$

$$+EA_0 U'(L) - 2kU(L) = -m\omega^2 U(L)$$

A 2-DOF system has the following equations of motion

$$m \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{Bmatrix} + k \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix} \begin{Bmatrix} x_1 \\ x_2 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

where  $m$  and  $k$  have units of kg and N/m, respectively. The system is given a set of initial conditions of  $x_1(0) = x_2(0) = x_0 = 0$  and  $\dot{x}_1(0) = \dot{x}_2(0) = v_0$ . Find  $\vec{x}(t)$ .

Bonus (3 points): If damping is added to the system the equation of motion can be written as

$$m \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{Bmatrix} + c \begin{bmatrix} 6 & -2 \\ -2 & 4 \end{bmatrix} + k \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix} \begin{Bmatrix} x_1 \\ x_2 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

Is the system proportionally damped? You must justify your answer to receive credit.

*assume  $\vec{x} = \vec{X} e^{-i\omega t}$ , 1st find natural frequencies and mode shapes*

*rewrite*

$$m \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{Bmatrix} + k \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix} \begin{Bmatrix} x_1 \\ x_2 \end{Bmatrix} = \vec{0} \quad \left( -\omega^2 \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} + \frac{k}{m} \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix} \right) \begin{Bmatrix} X_1 \\ X_2 \end{Bmatrix} = \vec{0}$$

$$\left( \begin{bmatrix} -2\omega^2 + 2k/m & -k/m \\ -k/m & -2\omega^2 + 2k/m \end{bmatrix} \right) \begin{Bmatrix} X_1 \\ X_2 \end{Bmatrix} = \vec{0}, \quad \text{next set determinant to 0}$$

$$(-2\omega^2 + 2k/m)(-2\omega^2 + 2k/m) - 3k^2/m^2 = 0$$

$$4\omega^4 - 4\omega^2 k/m - 4\omega^2 k/m - 3k^2/m^2 = 0 \quad \rightarrow$$

$$4\omega^4 - 8\omega^2 k/m - 3k^2/m^2 = 0$$

$$\omega^2 = \frac{-(-8)k/m \pm \sqrt{(-8k/m)^2 - 4(4)(-3)k^2/m^2}}{2(4)} =$$

$$\omega^2 = 1k/m \pm 1/8 \sqrt{16} k/m = (1 \pm 1/2) k/m$$

$$\omega^2 = 1/2 k/m, \quad 3/2 k/m \quad \rightarrow \quad \omega_1 = \sqrt{1/2} \sqrt{k/m} \quad \text{and} \quad \omega_2 = \sqrt{3/2} \sqrt{k/m}$$

$$\left( \begin{bmatrix} -2\omega^2 + 2k/m & -k/m \\ -k/m & -2\omega^2 + 2k/m \end{bmatrix} \right) \begin{Bmatrix} X_1 \\ X_2 \end{Bmatrix} = \vec{0} \quad \rightarrow \quad (-2\omega^2 + 2k/m)X_1 - (k/m)X_2 = 0$$

$$\frac{X_1}{X_2} = \frac{k/m}{2\omega^2 + 2k/m} \rightarrow \text{at } \omega = \omega_1 = \sqrt{1/2} \sqrt{k/m}$$

$$\frac{X_1^1}{X_2^1} = \frac{k/m}{-2(1/2)k/m + 2k/m} = \frac{1}{1} \rightarrow \vec{X}^1 = \begin{Bmatrix} 1 \\ 1 \end{Bmatrix}$$

$$\text{at } \omega = \omega_2 = \sqrt{3/2} \sqrt{k/m}$$

$$\frac{X_1^2}{X_2^2} = \frac{k/m}{-2(3/2)k/m + 2k/m} = \frac{-1}{1} \rightarrow \vec{X}^2 = \begin{Bmatrix} -1 \\ 1 \end{Bmatrix}$$

Evaluate  $c$  and  $s$  constants

$c_1$  and  $c_2$  are zero since  $\dot{\vec{x}}(0) = \vec{0}$

$$s_1 = \frac{\vec{X}^{1T} [M] \vec{x}(0)}{\omega_1 \vec{X}^{1T} [M] \vec{X}^1} = \frac{\begin{Bmatrix} 1 & 1 \end{Bmatrix}^T m \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} x_0 \\ v_0 \end{Bmatrix}}{\omega_1 \begin{Bmatrix} 1 & 1 \end{Bmatrix}^T m \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix}} = \frac{\begin{Bmatrix} 1 & 1 \end{Bmatrix}^T \begin{Bmatrix} 2v_0 \\ 2v_0 \end{Bmatrix}}{4\omega_1 \begin{Bmatrix} 1 & 1 \end{Bmatrix}^T \begin{Bmatrix} 2 \\ 2 \end{Bmatrix}} = \frac{4v_0}{4\omega_1} = \frac{v_0}{\omega_1}$$

$$s_2 = \frac{\vec{X}^{2T} [M] \vec{x}(0)}{\omega_2 \vec{X}^{2T} [M] \vec{X}^2} = \frac{\begin{Bmatrix} -1 & 1 \end{Bmatrix}^T m \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} x_0 \\ v_0 \end{Bmatrix}}{\omega_2 \begin{Bmatrix} -1 & 1 \end{Bmatrix}^T m \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} -1 \\ 1 \end{Bmatrix}} = \frac{\begin{Bmatrix} -1 & 1 \end{Bmatrix}^T \begin{Bmatrix} 2v_0 \\ 2v_0 \end{Bmatrix}}{\omega_2 \begin{Bmatrix} -1 & 1 \end{Bmatrix}^T \begin{Bmatrix} -2 \\ 2 \end{Bmatrix}} = \frac{0}{4\omega_2} = 0$$

$$\vec{x}(t) = c_1 \vec{X}^1 \sin \omega_1 t = \frac{v_0}{\omega_1} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix} \sin(\sqrt{1/2} \sqrt{k/m} t)$$

Bonus:  $[C] = \alpha[M] + \beta[K]$

$$c = \alpha(2) + \beta(2)$$

$$-2 = \alpha(0) + \beta(-1) \rightarrow \beta = 2 \quad \text{and} \quad \alpha = 1$$

$$\checkmark \checkmark \text{ with } 4 = \alpha(2) + \beta(2)$$

$$4 \neq 1(2) + 2(2) = 6$$

Not proportionally damped

A 2-DOF system has the following mass matrix:

$$m = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix}$$

with modal/natural frequencies of

$$\omega_1 = 0, \text{ rads/s} \quad \text{and} \quad \omega_2 = \sqrt{3} \text{ rads/s.}$$

In addition, the modes shapes are given by:

$$\vec{X}_1 = \begin{Bmatrix} 1 \\ 1 \end{Bmatrix}, \quad \text{and} \quad \vec{X}_2 = \begin{Bmatrix} 1 \\ -\frac{1}{2} \end{Bmatrix}$$

- Find the mass normalized modes shapes of the system.
- Use the mass normalized mode shapes to find the stiffness matrix of the system.

$$a) \quad d_1 = \frac{1}{\sqrt{\vec{X}_1^T [m] \vec{X}_1}} = \frac{1}{\sqrt{\begin{Bmatrix} 1 & 1 \end{Bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix}}} = \frac{1}{\sqrt{\begin{Bmatrix} 1 & 1 \end{Bmatrix} \begin{Bmatrix} 1 \\ 2 \end{Bmatrix}}} = \frac{1}{\sqrt{3}} = \frac{1}{\sqrt{3}}$$

$$\vec{\bar{X}}_1 = \frac{1}{\sqrt{3}} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix}$$

$$d_2 = \frac{1}{\sqrt{\vec{X}_2^T [m] \vec{X}_2}} = \frac{1}{\sqrt{\begin{Bmatrix} 1 & -1/2 \end{Bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} 1 \\ -1/2 \end{Bmatrix}}} = \frac{1}{\sqrt{\begin{Bmatrix} 1 & -1/2 \end{Bmatrix} \begin{Bmatrix} 1 \\ -1 \end{Bmatrix}}} = \frac{1}{\sqrt{1+1/2}} = \frac{1}{\sqrt{3/2}}$$

$$\vec{\bar{X}}_2 = \frac{1}{\sqrt{3/2}} \begin{Bmatrix} 1 \\ -1/2 \end{Bmatrix}$$

$$b) \quad \vec{\bar{X}}_1^T [K] \vec{\bar{X}}_1 = \omega_1^2 \quad \text{and} \quad \vec{\bar{X}}_2^T [K] \vec{\bar{X}}_2 = 0$$

$$\vec{\bar{X}}_2^T [K] \vec{\bar{X}}_2 = \omega_2^2 \quad [K] = \begin{bmatrix} k_{11} & k_{12} \\ k_{12} & k_{22} \end{bmatrix}$$

Expand  $\vec{\bar{X}}_1^T [K] \vec{\bar{X}}_1 = \omega_1^2$

$$\frac{1}{\sqrt{3m}} \begin{Bmatrix} 1 & 1 \end{Bmatrix} \begin{bmatrix} k_{11} & k_{12} \\ k_{12} & k_{22} \end{bmatrix} \frac{1}{\sqrt{3m}} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix} = \frac{1}{3m} \begin{Bmatrix} 1 & 1 \end{Bmatrix} \begin{Bmatrix} k_{11} + k_{12} \\ k_{12} + k_{22} \end{Bmatrix}$$

$$k_{11} + 2k_{12} + k_{22} = 0 \quad = \frac{1}{3} (k_{11} + 2k_{12} + k_{22}) = 0$$

Expand  $\vec{X}_2^T [K] \vec{X}_2 = \omega_2^2$

$$\frac{1}{\sqrt{3/2}} \left\{ 1 \quad -\frac{1}{2} \right\} \begin{bmatrix} K_{11} & K_{12} \\ K_{12} & K_{22} \end{bmatrix} \frac{1}{\sqrt{3/2}} \begin{Bmatrix} 1 \\ -1/2 \end{Bmatrix} = 3$$

$$\frac{2}{3} \left\{ 1 \quad -\frac{1}{2} \right\} \begin{Bmatrix} K_{11} - K_{12}/2 \\ K_{12} - K_{22}/2 \end{Bmatrix} = 3$$

$$\frac{2}{3} \left( K_{11} - K_{12}/2 - K_{12}/2 + K_{22}/4 \right) = 3$$

$$K_{11} - K_{12} + K_{22}/4 = 9/2$$

Expand  $\vec{X}_2' [K] \vec{X}_1 = 0$

$$\frac{1}{\sqrt{3/2}} \left\{ 1 \quad -\frac{1}{2} \right\} \begin{bmatrix} K_{11} & K_{12} \\ K_{12} & K_{22} \end{bmatrix} \frac{1}{\sqrt{3}} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix} = 0$$

$$\frac{1}{\sqrt{6/2}} \left\{ 1 \quad -\frac{1}{2} \right\} \begin{Bmatrix} K_{11} + K_{12} \\ K_{12} + K_{22} \end{Bmatrix} = 0$$

$$K_{11} + K_{12} - K_{12}/2 - K_{22}/2 = 0$$

$$K_{11} + 3K_{12}/2 - K_{22}/2 = 0$$

You have 3 equations and 3 unknowns

$$K_{11} + 2K_{12} + K_{22} = 0$$

$$K_{11} - K_{12} + K_{22}/4 = 9/2$$

$$K_{11} + 3K_{12}/2 - K_{22}/2 = 0$$

$$K_{11} = 2 \quad K_{12} = -2 \quad K_{22} =$$