

## Test 1

Name KEY

Pledge \_\_\_\_\_

*I have neither given nor received aid on this examination.*

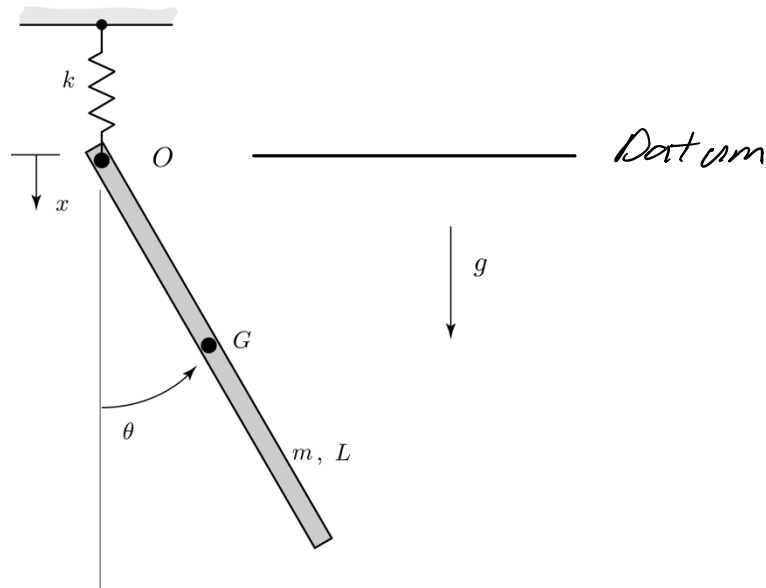
### **Instructions:**

- This is a closed-book, closed-notes exam.
- You are NOT allowed to use a programmable calculator during the exam.
- Please read the question on this exam carefully and answer only the questions I ask. Don't waste your time doing extra work, and don't skip any of the smaller questions within a problem. I can't grade what I can't see and I can't give partial credit for something in your head.

**ME 563 - Fall 2020**  
**Test Problem 1 -30points**

Name \_\_\_\_\_

A bar is attached to a spring at pt  $O$ . The spring is constrained to deform purely in vertical ( $x$ ) direction. The bar has mass  $m$  and mass moment of inertia about its center of gravity of  $I^G = 1/12mL^2$ . The coordinate  $x$  denotes the absolute position of the roller and  $\theta$  the angular position of the bar.



- Determine the expression for potential energy  $U$  in terms of the generalized coordinates  $x$  and  $\theta$  and determine the equilibrium positions of the system.
- Write down an expression for the kinetic energy  $T$  in terms of the generalized coordinates  $x$  and  $\theta$  and their time derivatives. From this expression, identify the elements  $m_{ij}$ , where:

$$T = \frac{1}{2} \sum_{i=1}^2 \sum_{j=1}^2 m_{ij} \dot{q}_i \dot{q}_j$$

- Determine the mass matrix  $[M]$  and the stiffness matrix  $[K]$  corresponding small oscillations about the equilibrium state.

a)  $U = \frac{1}{2} kx^2 - mg(x + \frac{L}{2} \cos \theta)$

$\frac{\partial U}{\partial x} = kx - mg, \quad \frac{\partial U}{\partial \theta} = mg \frac{L}{2} \sin \theta$

$\left. \frac{\partial U}{\partial q} \right|_{\vec{q}_e} = \vec{0}$

$\left\{ \begin{matrix} \frac{\partial U}{\partial x} \\ \frac{\partial U}{\partial \theta} \end{matrix} \right\} = \vec{0}$

1)  $kx = mg, \quad x_e = mg/k$   
 2)  $mg \frac{L}{2} \sin \theta = 0, \quad \theta_e = n\pi$   
 $n = 0, 1, 2, 3, \dots$

$x_e = 0, \text{ and } \theta_e = n\pi, \quad n = 0, 1, 2, 3, \dots, \infty$

## Test Problem 1 Additional Page

b)

$$\vec{r}_0 = x \hat{i}, \quad \vec{r}_{c/o} = L/2 \cos \theta \hat{i} + L/2 \sin \theta \hat{j},$$

$$\vec{r}_c = \vec{r}_0 + \vec{r}_{c/o} = (x + L/2 \cos \theta) \hat{i} + L/2 \sin \theta \hat{j}$$

$$\dot{\vec{r}}_c = (\dot{x} - \dot{\theta} L/2 \sin \theta) \hat{i} + \dot{\theta} L/2 \cos \theta \hat{j}$$

$$T = \frac{1}{2} m \dot{\vec{r}}_c \cdot \dot{\vec{r}}_c + \frac{1}{2} I_c \dot{\theta}^2 = \frac{1}{2} m (\dot{x}^2 - \dot{x} \dot{\theta} L \sin \theta + \dot{\theta}^2 L^2/4) + \frac{1}{2} m L^2 \dot{\theta}^2$$

$$m_{11} = m,$$

$$m_{12} = m_{21} = -\frac{mL}{2} \sin \theta, \text{ and}$$

$$m_{22} = mL^2/4$$

$$c) [m] = m \begin{bmatrix} 1 & 0 \\ -L/2 \sin(n\pi) & L^2/4 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & L^2/3 \end{bmatrix}$$

$$k_{11} = \left. \frac{\partial^2 U}{\partial x^2} \right|_{\vec{q}_e} = k, \quad k_{12} = \left. \frac{\partial^2 U}{\partial x \partial \theta} \right|_{\vec{q}_e} = k_{21} = 0$$

$$k_{22} = \left. \frac{\partial^2 U}{\partial \theta^2} \right|_{\vec{q}_e} = mgL/2 \cos(n\pi) = mgL/2 (-1)^n$$

$$k = \begin{bmatrix} k & 0 \\ 0 & mgL/2 (-1)^n \end{bmatrix} = \begin{bmatrix} k & 0 \\ 0 & (-1)^n mgL/2 \end{bmatrix}$$

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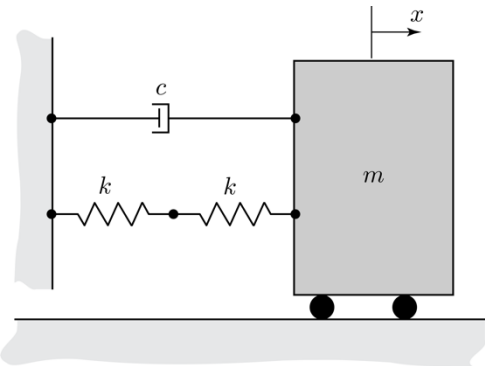
**Name** \_\_\_\_\_

**Test Problem 1 Additional Page**

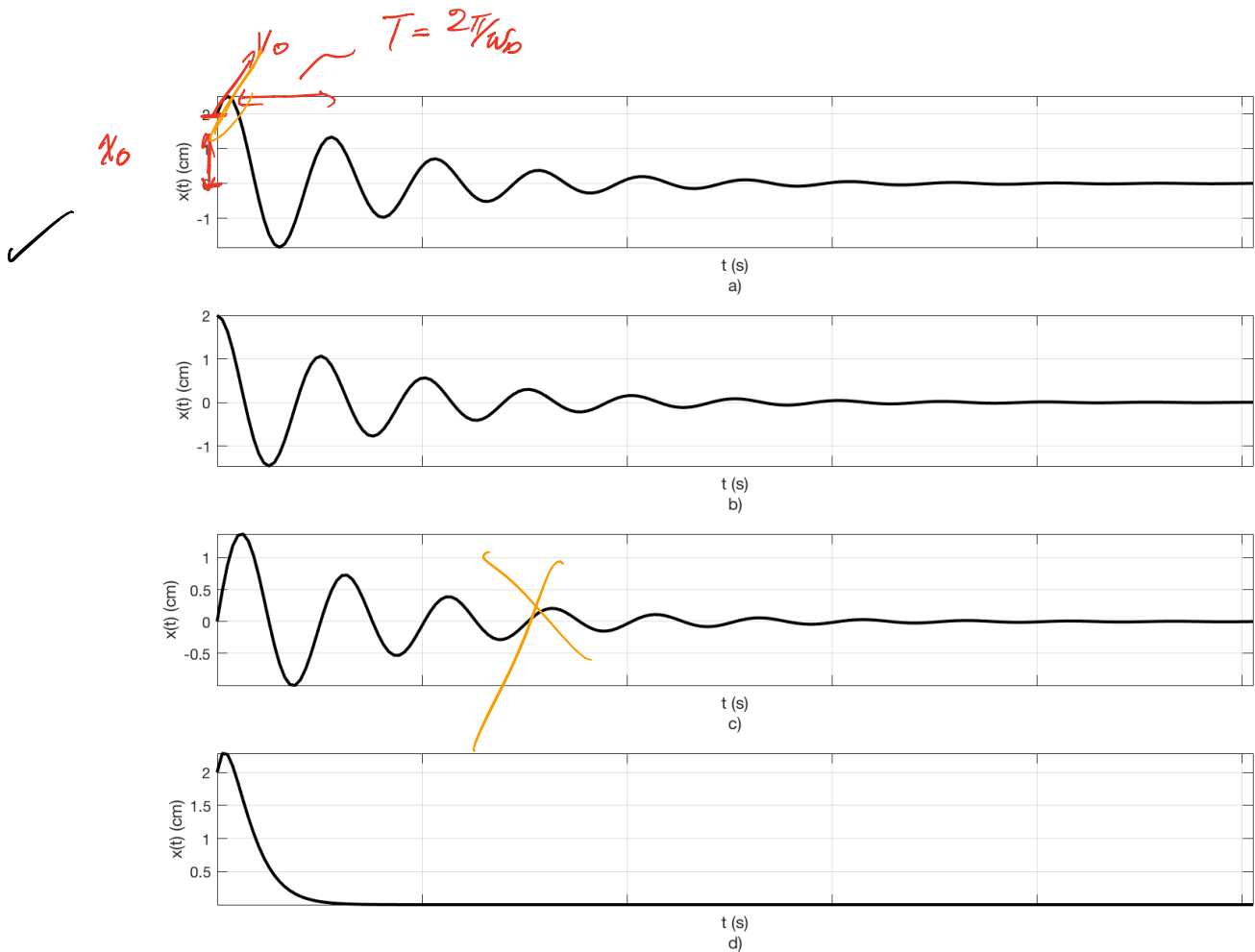
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**Test Problem 2 -20 points**

Name \_\_\_\_\_

A single degree of freedom systems has system parameters of  $m = 100$  kg,  $k = 25\sqrt{2}$  N/m, and  $c = 50$  kg/s, The system has initial condition  $x_0 = 2$ cm, and  $v_0 = 4$ cm/s.



- Determine the natural frequency of the system.
- Determine the damping ratio of the system.
- Determine the damped natural frequency of the system.
- Indicate the correct plot of the response of system. On this label the initial conditions and the period of oscillations of the system, and the length of the period.



a)  $\frac{1}{k_{eq}} = \frac{1}{k} + \frac{1}{k} \rightarrow k_{eq} = \frac{k^2}{k_2} = \frac{k}{2} = \frac{25\sqrt{2}}{2} \text{ N/m} = 17.67 \text{ N/m}$

$\omega_n = \sqrt{k_{eq}/m} = \sqrt{25\sqrt{2}/2 \cdot 100} = \sqrt{\frac{\sqrt{2}}{8}} = \underline{0.4204 \text{ rad/s}}$

## Test Problem 2 Additional Page

$$b) \quad 2\zeta\omega_n = c/m$$

$$\zeta = \frac{c}{2m\omega_n} = \frac{c}{2m\sqrt{k_{eq}/m}} = \frac{c}{2\sqrt{mk_{eq}}}$$

$$= \frac{c}{2\sqrt{mk/2}} = \frac{50}{2\sqrt{100(25\sqrt{2}/2)}} = \underline{0.5946}$$

*underdamped*

$$c) \quad \omega_0 = \omega_n \sqrt{1-\zeta^2} = 0.424 \sqrt{1-0.5946^2} = \underline{0.3380 \text{ rad/s}}$$

A 2-DOF system has the follow equations of motion.

$$m \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{Bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{Bmatrix} + k \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} x_1 \\ x_2 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

Determine the natural frequencies and mode shapes of the system.

Assume  $\vec{x} = \vec{X} e^{i\omega t} = \vec{X} e^{i\omega t}$

$$[m]\ddot{\vec{x}} + [k]\vec{x} = \vec{0} \rightarrow (-\omega^2[m] + [k])\vec{X} e^{i\omega t} = \vec{0}$$

Natural Frequencies

$$\begin{bmatrix} -\omega^2 m + k & -k \\ -k & -\omega^2 m + k \end{bmatrix} \begin{Bmatrix} X_1 \\ X_2 \end{Bmatrix} = \vec{0}$$

$$(-\omega^2 m + k)^2 - (k)^2 = (\omega^4 m^2 - \omega^2(2mk) + k^2 - k^2) = 0$$

$$\omega^4 - 2mk\omega^2 = \omega^2(\omega^2 m^2 - 2mk) = 0$$

$$\omega^2 = 0 \quad \omega^2 m^2 - 2mk = 0$$

$\omega = 0$  and  $\omega = \sqrt{2} \sqrt{k/m}$   $\sim$  Rigid body mode  $\omega = 0$

Modal Shapes

$$(-\omega^2 m + k)X_1 - kX_2 = 0 \rightarrow \frac{X_2}{X_1} = \frac{\omega^2 m + k}{k} = -\omega^2 m/k + 1$$

$$\vec{X} = \begin{Bmatrix} 1 \\ \omega^2 m/k + 1 \end{Bmatrix} \quad \omega = 0, \vec{X} = \begin{Bmatrix} 1 \\ 1 \end{Bmatrix}, \quad \omega = \sqrt{2} \sqrt{k/m}, \vec{X} = \begin{Bmatrix} 1 \\ -1 \end{Bmatrix}$$

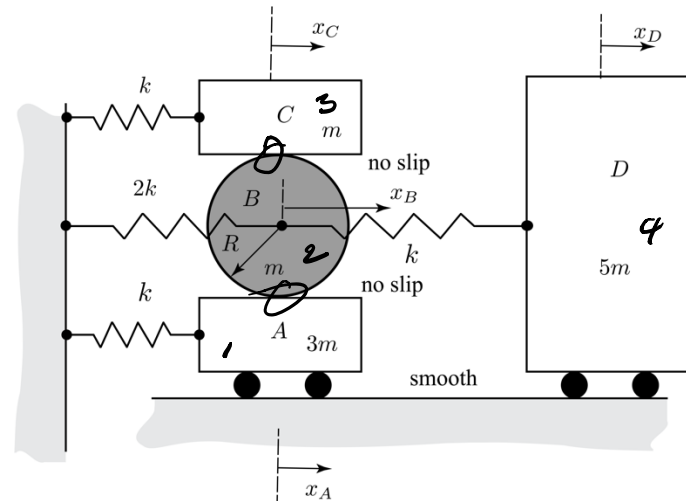
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**Test Problem 3 Additional Page**

**Name** \_\_\_\_\_

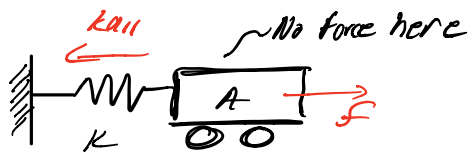


Consider the system below, whose motion is described by the absolute coordinates shown. Use the method of influence coefficients to develop the flexibility matrix  $[A] = [K]^{-1}$ .

Numbering to Letters  
 A → 1  
 B → 2  
 C → 3  
 D → 4



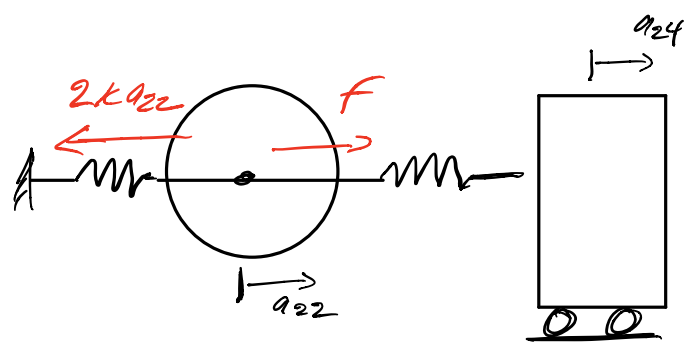
Apply a unit load @ "A"



~ No force here  
 $\sum F_x: -ka_{11} + F = 0, \quad a_{11} = 1/k$   
 $a_{12} = a_{13} = a_{14} = 0$

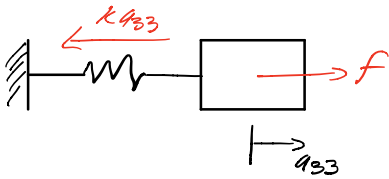
By reciprocity  $a_{12} = a_{21} = 0, \quad a_{13} = a_{31} = 0, \quad a_{14} = a_{41} = 0$

Apply unit load @ "B"



$\sum F_x: -2ka_{22} + F = 0, \quad a_{22} = 1/2k$   
 $a_{23} = 0 \quad a_{32} = a_{23} = 0$   
 $a_{21} = 0$   
 $a_{24} = a_{22} = a_{42} = 1/2k$

Apply unit load @ "C"

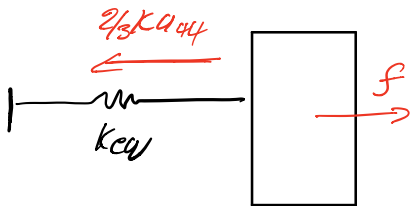


$$a_{34} = 0 \quad a_{31} = 0, \quad a_{32} = 0$$

$$a_{43} = a_{13} = a_{23} = 0$$

$$\pm \sum F_x: -k_{433} + f = 0$$

$$a_{33} = \frac{1}{k}$$



$$\frac{1}{k_{eq}} = \frac{1}{k} + \frac{1}{2k}$$

$$\frac{1}{k_{eq}} = \frac{1}{k} \left( \frac{2k}{2k} \right) + \left( \frac{1}{2k} \right) \left( \frac{k}{k} \right)$$

$$\frac{1}{k_{eq}} = \frac{3k}{2k^2} \quad k_{eq} = \frac{2}{3}k$$

$$\pm \sum F_x: -\frac{2}{3}k_{444} + f = 0$$

$$a_{44} = \frac{3}{2}k$$

In summary,

$$a_{11} = \frac{1}{k}, \quad a_{12} = 0, \quad a_{13} = 0, \quad a_{14} = 0$$

$$a_{21} = 0, \quad a_{22} = \frac{1}{2}k, \quad a_{23} = 0, \quad a_{24} = \frac{1}{2}k$$

$$a_{31} = 0, \quad a_{32} = 0, \quad a_{33} = \frac{1}{k}, \quad a_{34} = 0$$

$$a_{41} = 0, \quad a_{42} = \frac{1}{2}k, \quad a_{43} = 0, \quad a_{44} = \frac{3}{2}k$$

$$[a] = \begin{bmatrix} \frac{1}{k} & 0 & 0 & 0 \\ 0 & \frac{1}{2}k & 0 & \frac{1}{2}k \\ 0 & 0 & \frac{1}{k} & 0 \\ 0 & \frac{1}{2}k & 0 & \frac{3}{2}k \end{bmatrix}$$