

**Problem 7.1 (10 points)**

Three different shafts made up of the same material with shear modulus  $G$  are connected through connectors  $B$  and  $C$ . Shaft (1) is a hollow shaft with outer and inner diameters of  $3d$  and  $d$  while shafts (2) and (3) are rigid shafts with diameters of  $2d$  and  $d$  respectively. This system of shafts is subjected to external torques  $T_0$  (applied on connector  $B$ ) and  $T$  (applied on connector  $C$ ). The configuration of the system is shown in Figure 1. Assume shafts and connectors are weightless.

- a) Write down the strain-energy equation of the system.
- b) Calculate the static rotations of connectors  $B$  and  $C$  using *Castigliano's theorem*.

Write your answer in terms of, at most,  $T_0$ ,  $T$ ,  $L$ ,  $d$ , and  $G$ .

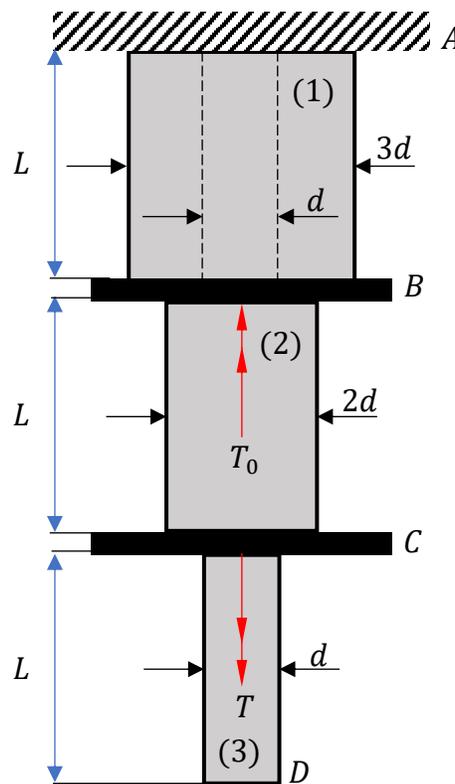


Figure 1

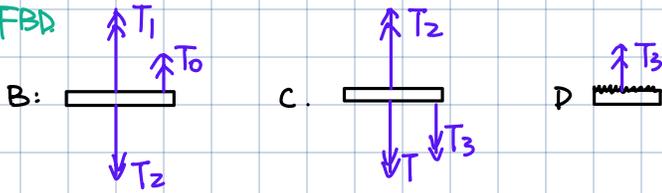
Given:  $T_0, T, L, d, G$

Find:  $\phi_B, \phi_C$

Solution:

1. Coord.  $\downarrow x^+$

2. FBD



3. Equilibrium Equation

$$T_2 - T_0 - T_1 = 0 \quad (1)$$

$$T + T_3 - T_2 = 0 \quad (2)$$

$$T_3 = 0 \quad (3)$$

unknown:  $T_1, T_2, T_3$

3 unknown. 3 Eq.

4. Energy method.

Solve for  $T_1, T_2, T_3$

$$T_3 = 0$$

$$T_2 = T$$

$$T_1 = T_2 - T_0 = T - T_0$$

Strain Energy function.

$$U = \frac{1}{2} \frac{T_1^2 L}{J_1 G} + \frac{1}{2} \frac{T_2^2 L}{J_2 G} + \frac{1}{2} \frac{T_3^2 L}{J_3 G}$$

$$= \frac{L}{2 G \pi d^4} \left[ \frac{1}{5} T_1^2 + 2 T_2^2 + \frac{16}{32} T_3^2 \right]$$

$$= \frac{L}{G \pi d^4} \left[ \frac{1}{5} T^2 + \frac{1}{5} T_0^2 - \frac{2}{5} T T_0 + T^2 \right]$$

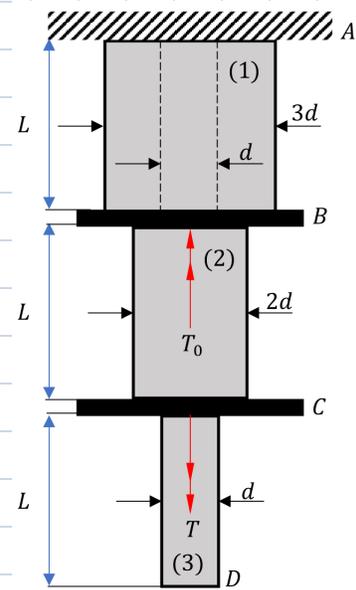
$$= \frac{L}{G \pi d^4} \left[ \frac{6}{5} T^2 - \frac{2}{5} T T_0 + \frac{1}{5} T_0^2 \right]$$

$\phi_B$  (same direction as  $T_0$ )

$$\phi_B = \frac{\partial U}{\partial T_0} = \frac{L}{G \pi d^4} \left[ -\frac{2}{5} T + \frac{2}{5} T_0 \right] = \frac{2L(T_0 - T)}{5G \pi d^4} \quad \uparrow$$

$\phi_C$  (same direction as  $T$ )

$$\phi_C = \frac{\partial U}{\partial T} = \frac{L}{G \pi d^4} \left[ \frac{12}{5} T - \frac{2}{5} T_0 \right] = \frac{L(12T - 2T_0)}{5G \pi d^4} \quad \downarrow$$



$$J_1 = \frac{\pi}{2} \left[ \left(\frac{3d}{2}\right)^4 - \left(\frac{d}{2}\right)^4 \right]$$

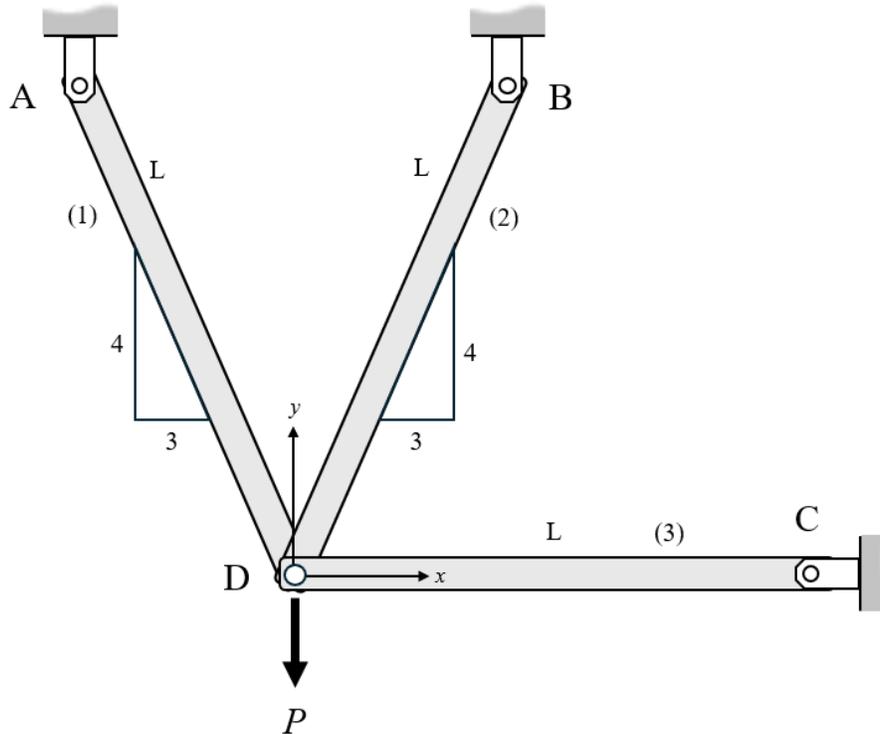
$$= \frac{80\pi d^4}{32} = \frac{5}{2} \pi d^4$$

$$J_2 = \frac{\pi}{2} d^4$$

$$J_3 = \frac{\pi}{2} \cdot \left(\frac{d}{2}\right)^4 = \frac{\pi}{32} d^4$$

**Problem 7.2 (10 points)**

Consider the truss depicted below. All members have a cross-sectional area  $A$ , length  $L$ , and Young's modulus  $E$ . A load  $P$  is applied at  $D$  as shown. Use energy methods to solve this problem.



Follow the steps provided below to determine the vertical displacement of pin D:

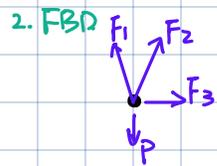
- (a) Draw the necessary free body diagram(s).
- (b) Write down the corresponding equilibrium equations.
- (c) Determine whether the structure is determinate or indeterminate.
- (d) State your choice for redundant load(s), if needed.
- (e) State your choice for dummy load(s), if needed.
- (f) Determine the elastic strain energy of beams 1, 2, and 3 in terms of  $P$ ,  $E$ ,  $L$ ,  $A$ , and the redundant load(s).
- (g) Determine the axial loads in the three elements using Castigliano's second theorem.
- (h) Use Castigliano's second theorem to determine the vertical displacement of pin D.

Express your results in terms of  $P$ ,  $E$ ,  $L$ , and  $A$ .

Given: A. E. L. P.

Find:  $F_1, F_2, F_3, v_D$ .

Solution: 1. Coord (given)



3. Equilibrium Equation.

$$F_x: -\frac{3}{5}F_1 + \frac{3}{5}F_2 + F_3 = 0$$

$$F_y: \frac{4}{5}F_1 + \frac{4}{5}F_2 - P = 0$$

3 unknowns:  $F_1, F_2, F_3$ .

2 Equation  $\Rightarrow$  Indeterminate.

4. Energy method.

$$U = U_1 + U_2 + U_3$$

$$= \frac{1}{2} \cdot \frac{F_1^2 L}{EA} + \frac{F_2^2 L}{EA} + \frac{F_3^2 L}{EA}$$

$$= \frac{L}{2EA} (F_1^2 + F_2^2 + F_3^2)$$

choose  $F_3$  as redundant force.

$$\textcircled{2} \rightarrow F_1 = \frac{5}{4}P - F_2$$

$$\textcircled{1} \rightarrow -\frac{3}{4}P + \frac{3}{5}F_2 + \frac{3}{5}F_2 + F_3 = 0$$

$$\frac{6}{5}F_2 = \frac{3}{4}P - F_3$$

$$F_2 = \frac{5}{8}P - \frac{5}{6}F_3$$

$$F_1 = \frac{5}{4}P - \frac{5}{8}P + \frac{5}{6}F_3$$
$$= \frac{5}{8}P + \frac{5}{6}F_3$$

Write U w/ Redundant load.

$$U = \frac{L}{2EA} \left[ \left( \frac{5}{8}P + \frac{5}{6}F_3 \right)^2 + \left( \frac{5}{8}P - \frac{5}{6}F_3 \right)^2 + F_3^2 \right]$$

$$= \frac{L}{2EA} \left[ \frac{25}{32}P^2 + \frac{25}{18}F_3^2 + F_3^2 \right]$$

$$= \frac{L}{2EA} \left[ \frac{25}{32}P^2 + \frac{43}{18}F_3^2 \right]$$

w/ Redundant load,  $\frac{\partial U}{\partial F_3} = 0$

$$\frac{\partial U}{\partial F_3} = \frac{L}{2EA} \cdot \frac{43}{18} \cdot 2F_3 = 0 \Rightarrow F_3 = 0$$

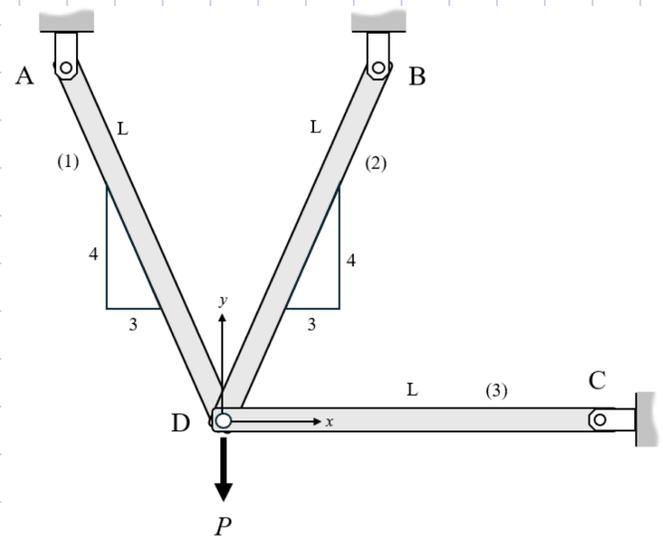
Find  $F_1, F_2$  from Equilibrium Eq:

$$F_1 = \frac{5}{8}P, \quad F_2 = \frac{5}{8}P$$

For vertical displacement  $v_D$ ,

$v_D$  in same direction as P

no dummy load needed.



$$\text{Find } v_D = \frac{\partial U}{\partial P}$$

$$v_D = \frac{\partial U}{\partial P} = \frac{L}{2EA} \cdot \frac{25}{32} \cdot 2P = \frac{25PL}{32EA}$$

$$v_D = \frac{25PL}{32EA} \downarrow$$

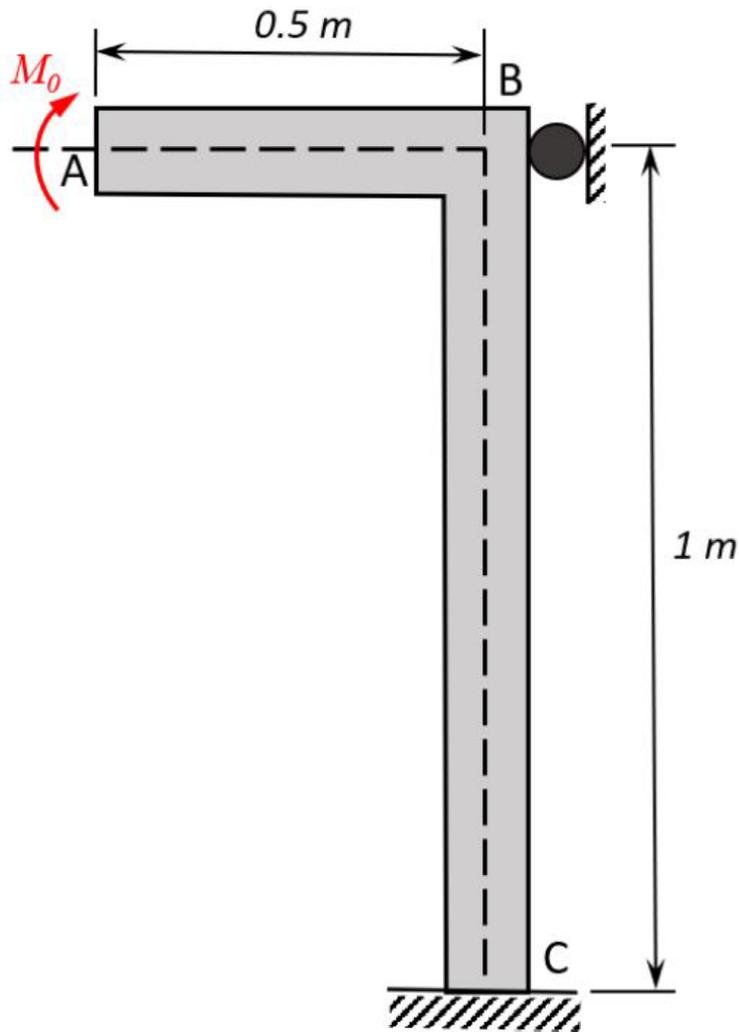
**Problem 7.3 (10 points)**

Two segments, AB and BC, with a thin walled hollow circular cross section of outer diameter  $a$  and inner diameter  $0.8a$ , are welded together at B to form the L-shaped ABC shown in the figure below. Shear strain energy due to bending can be neglected.

Use the following data in your analysis:  $E = 280 \text{ GPa}$ ,  $G = 120 \text{ GPa}$ ,  $a = 20 \text{ mm}$ ,  $M = 1000 \text{ Nm}$

(a) Determine the reactions.

(b) Use Castigliano's Second Theorem to determine the vertical displacement at point A,  $v_A$ .



Given: thin wall circ.  $d_o = 20 \text{ mm}$ ,  $d_i = 16 \text{ mm}$ .

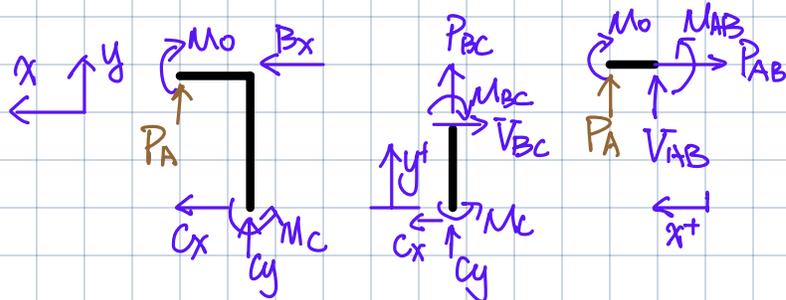
$$E = 280 \text{ GPa} = 2.8 \times 10^{11} \text{ Pa}$$

$$G = 120 \text{ GPa} = 1.2 \times 10^{11} \text{ Pa}$$

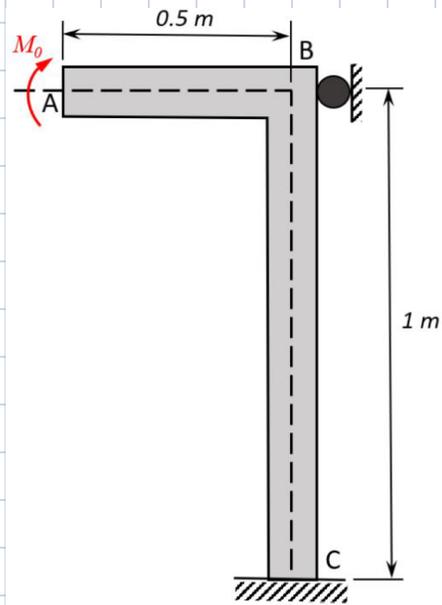
$$M_o = 10^3 \text{ N}\cdot\text{m} \quad \text{Ignore } U_T$$

Find:  $C_x, C_y, M_c, B_x, \delta_A$

Solution: 1. coord and FBD.



\* PA is dummy load @ A since need to find  $\delta_A$  in y direction.



## 2. Equilibrium Eq.

$$\text{ABC: } B_x + C_x = 0$$

$$C_y + P_A = 0$$

$$M_c - M_o + (1 \text{ m})B_x - P_A(0.5 \text{ m}) = 0$$

$$\text{BC segment: } C_y + P_{bc} = 0$$

$$C_x - V_{bc} = 0$$

$$M_c - M_{bc} - C_x \cdot y$$

$$\text{AB segment: } -P_{AB} = 0$$

$$P_A + V_{AB} = 0$$

$$-M_o + M_{AB} - P_A(0.5 \text{ m} - x) = 0$$

## 3. Internal Reaction

Statically Indeterminate.

Redundant Support:  $C_x$ .

$$B_x = -C_x$$

$$C_y = -P_A$$

$$M_c = M_o - (-C_x) = M_o + C_x(1 \text{ m}) + 0.5 P_A$$

$$\text{Seg BC: } P_{bc} = -C_y$$

$$M_{bc} = -C_x \cdot y + M_o + C_x(1 \text{ m})$$

$$M_{bc}(y) = -C_x y + (10^3 + C_x + 0.5 P_A)$$

$$\text{Seg AB: } P_{AB} = 0$$

$$M_{AB}(x) = M_o + P_A(0.5 \text{ m} - x)$$

$$M_{AB}(x) = -P_A x + (0.5 P_A + 10^3)$$

$$A = \pi [(10^{-2} \text{ m})^2 - (8 \times 10^{-3})^2] = 36\pi \times 10^{-6} \text{ m}^2 = 1.13 \times 10^{-4} \text{ m}^2$$

$$I = \frac{\pi}{2} [(10^{-2} \text{ m})^4 - (8 \times 10^{-3})^4] = 292\pi \times 10^{-12} \text{ m}^4 = 9.273 \times 10^{-9} \text{ m}^4$$

## 4. Strain Energy

seg. BC: ( $P_{bc}, M_{bc}(y)$ )

$$U_{BCP} = \frac{C_y^2 \cdot L}{2EA} = \frac{C_y^2}{2 \times 2.8 \times 10^{11} \cdot 1.13 \times 10^{-4}} = 0.158 \cdot 10^{-7} P_A^2$$

$$U_{BCM} = \frac{1}{2EI} \int_0^{1 \text{ m}} (-C_x y + C_x + 10^3 + 0.5 P_A)^2 dy$$

$$= \frac{\frac{1}{2} C_x^2 y^2 + 0.5 C_x P_A y + 10^3 C_x y + 0.25 (P_A + 10^3)^2 y^2}{2 \times 2.8 \times 10^{11} \times 9.273 \times 10^{-9}}$$

$$= 6.42 \times 10^{-5} C_x^2 + 0.1926 C_x + 9.63 \times 10^{-5} C_x P_A + 4.81 \times 10^{-5} P_A^2 + 0.1926 P_A + 192.6$$

seg. AB: ( $P_{AB}, M_{AB}(x)$ )

$$U_{ABP} = 0 \quad (P_{AB} = 0)$$

$$U_{ABM} = \frac{1}{EI} \int_0^{0.5 \text{ m}} [-P_A x + (0.5 P_A + 10^3)]^2 dx$$

$$= \frac{1}{2 \times 2.8 \times 10^{11} \times 9.273 \times 10^{-9}} \left[ \frac{1}{24} P_A^2 + 250 P_A + 5 \times 10^5 \right]$$

$$= 8.024 \times 10^{-6} P_A^2 + 4.814 \times 10^{-2} P_A + 96.29$$

Total U

$$U = U_{BCP} + U_{BCM} + U_{ABP} + U_{ABM}$$

$$= 6.42 \times 10^{-5} C_x^2 + 9.628 \times 10^{-5} C_x P_A + 0.1926 C_x + 5.632 \times 10^{-5} P_A^2 + 0.2407 P_A + 288.86$$

Continue to next page.

## 5. Reactions:

Redundant support:  $C_x$ . w/  $P_A = 0$

$$\frac{\partial U}{\partial C_x} = 0 \Rightarrow \frac{\partial U}{\partial C_x} = 2 \times 6.42 \times 10^{-5} C_x + 0.1926 = 0 \Rightarrow C_x = -1500 \text{ N.}$$

w/ Equilibrium  $E_B$  and  $P_A = 0$ .

$$B_x = -C_x = 1500 \text{ N}$$

$$C_y = 0 \text{ N.}$$

$$M_C = M_0 - B_x \cdot 1 \text{ m} = 1000 \text{ N} \cdot \text{m} - 1500 \text{ N} \cdot 1 \text{ m} = -500 \text{ N} \cdot \text{m}$$

Reaction @ B:  $\leftarrow 1500 \text{ N}$

@ C:  $\rightarrow 1500 \text{ N}$

$\curvearrowright 500 \text{ N} \cdot \text{m}$

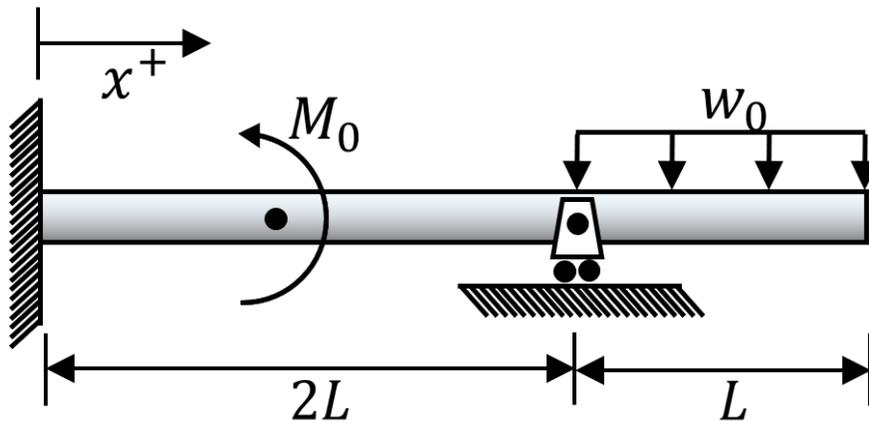
## 6. Displacement @ A.

$$\begin{aligned} v_A \text{ in } y &= \frac{\partial U}{\partial P_A} = 9.628 \times 10^{-5} C_x + 2 \cdot 5.632 \times 10^{-5} P_A + 0.2407 \\ &= 9.628 \times 10^{-5} \cdot (-1500 \text{ N}) + 0.2407 \\ &= 0.09627 \text{ m} \end{aligned}$$

$v_A$  in same direction as  $P_A$ .

$v_A \uparrow 0.09627 \text{ m}$

**Problem 7.4 (5 points)**



**Problem 7.4.1 (2.5 points)**

Refer to the figure above. For the given loads and supports, which of the following is the correct breakdown of the system if the deflection was to be calculated with the Superposition principle?

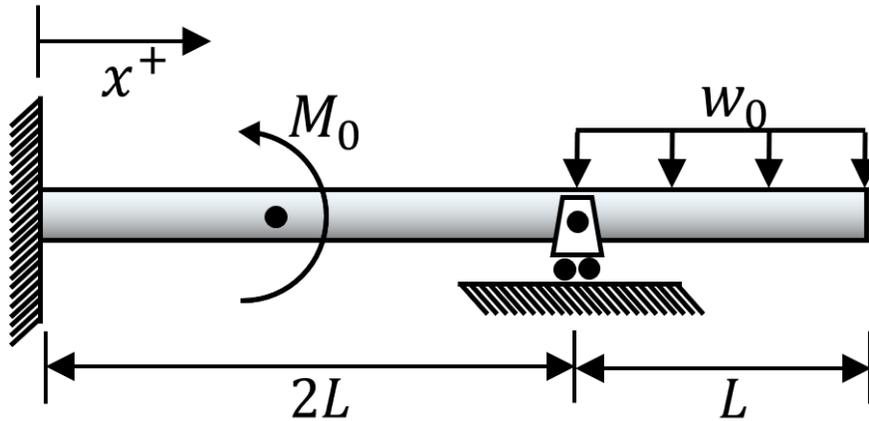
- A)
- B)
- C)
- D)

**Problem 7.4.2 (2.5 points)**

Which of the following represent the correct set of boundary conditions applied to the beam?

- A)  $v(0) = 0, v'(0) = 0, v(2L) = 0, v'(2L) = 0$
- B)  $v(0) = 0, v'(0) = 0, v(2L) = 0$
- C)  $v(0) = 0, v'(0) = 0, v'(2L) = 0$
- D)  $v(0) = 0, v'(0) = 0$

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- D)  $v(0) = 0, v'(0) = 0$

*w/  $x=0, v=0, v'=0$*

*w/  $x=2L, v=0, v'$  unknown.*