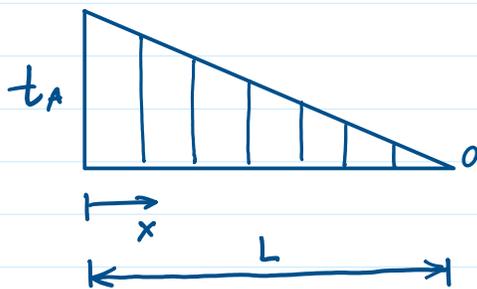
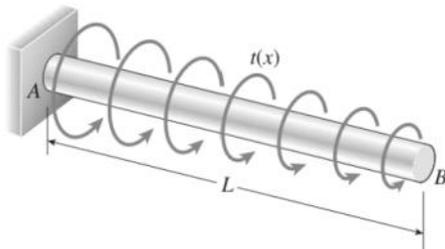


Problem 1.

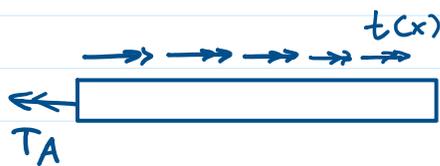
A solid prismatic bar AB of uniform circular cross section (diameter d) is loaded by a distributed torque (see figure). The intensity of the distributed torque, that is, the torque per unit distance, is denoted $t(x)$ (Nm/m) and varies linearly from a maximum value t_A at end A to zero at end B. Also, the length of the bar is L and the shear modulus of elasticity of the material is G .

- (a) Determine the maximum shear stress τ_{max} in the bar.
- (b) Determine the angle of twist ϕ between the ends of the bar.



$$t(x) = t_A - \frac{t_A x}{L} \quad \left(\frac{Nm}{m}\right)$$

FBD:



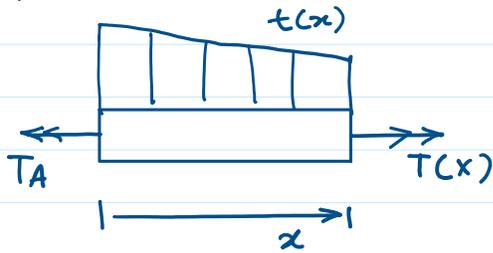
$$\sum T = 0 \quad \therefore \quad -T_A + \int_0^L t(x) dx = 0$$

$$-T_A + \int_0^L \left(t_A - \frac{t_A x}{L} \right) dx = 0$$

$$T_A = \frac{t_A L}{2} \quad (N \cdot m)$$

Section at x .

Section at x .



$$\sum T = 0$$

$$-T_A + \int_0^x t(\xi) d\xi + T(x) = 0$$

$$T(x) = \frac{t_A x^2}{2L} - t_A x + \frac{t_A L}{2}$$

$$T_{\max} = \frac{t_A L}{2} \quad @ \quad x = 0$$

$$\begin{aligned} \tau_{\max} &= \frac{T_{\max} \cdot r}{I_p} \\ &= \frac{t_A L \cdot d}{4 \cdot \frac{\pi \cdot d^4}{32}} \end{aligned}$$

$$I_p = \frac{\pi r^4}{2} \quad \text{or} \quad \frac{\pi d^4}{32}$$

$$\tau_{\max} = \frac{8 t_A L}{\pi d^3}$$

(b) ϕ :

$$\frac{d\phi}{dx} = \frac{T(x)}{GI_p}$$

$$\phi = \int_0^L \frac{T(x)}{GI_p} dx = \frac{1}{GI_p} \int_0^L \left(\frac{t_A x^2}{2L} - t_A x + \frac{t_A L}{2} \right) dx$$

$$\phi = \frac{32}{G \cdot \pi d^4} \cdot \frac{t_A L^2}{6}$$

$$\phi = \frac{16 t_A L^2}{3 \pi G d^4}$$

Problem 2:

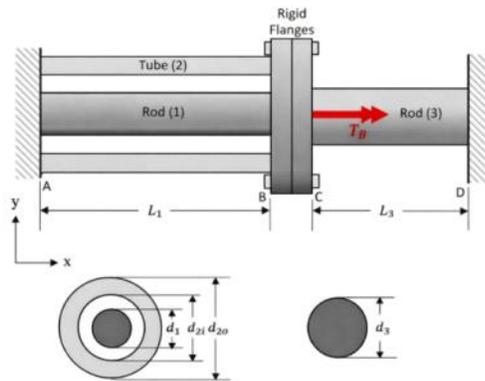
A solid rod (1) of diameter d_1 is enclosed by a concentric tube (2) of inner diameter d_{2i} and outer diameter d_{2o} , and both are attached to a rigid support at A and a rigid flat flange at B. A solid rod (3) of diameter d_3 is similarly attached to a rigid support at D and a rigid flat flange at C. The flanges are securely connected. Subsequently, an external torque T_B is applied at B.

- Determine the internal torques T_1 , T_2 , T_3 in three elements resulting from the load T_B
- Determine the maximum shear stresses $\tau_{\max(1)}$, $\tau_{\max(2)}$, $\tau_{\max(3)}$ in the three elements.
- Determine the angle of twist at the rigid flanges (B or C)

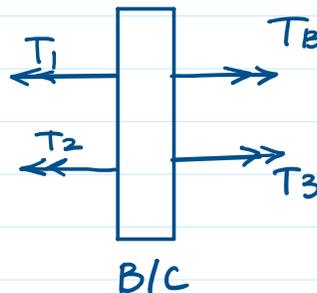
Given: $d_1 = 3 \text{ cm}$, $d_{2i} = 4 \text{ cm}$, $d_{2o} = 5 \text{ cm}$, $d_3 = 3.5 \text{ cm}$,

$G_1 = 20 \text{ GPa}$, $G_2 = 10 \text{ GPa}$, $G_3 = 30 \text{ GPa}$,

$L_1 = 200 \text{ cm}$, $L_3 = 100 \text{ cm}$, $T_B = 100 \text{ N m}$



FBD.



$$\sum T: T_1 + T_2 = T_3 + T_B \rightarrow \textcircled{1}$$

3 unknowns, 1 equation.

Compatibility conditions:

$$\Delta\phi_1 = \Delta\phi_2 \rightarrow \textcircled{2}$$

$$\Delta\phi_1 + \Delta\phi_3 = 0 \rightarrow \textcircled{3}$$

$$\Delta\phi_1 = \frac{T_1 L_1}{G_1 J_1} \quad \Delta\phi_2 = \frac{T_2 L_2}{G_2 J_2} \quad \Delta\phi_3 = \frac{T_3 L_3}{G_3 J_3}$$

$$\Delta\phi_1 = \frac{T_1 L_1}{G_1 I_{p1}} \quad \Delta\phi_2 = \frac{T_2 L_2}{G_2 I_{p2}} \quad \Delta\phi_3 = \frac{T_3 L_3}{G_3 I_{p3}}$$

Substituting into (2) and (3)

$$\frac{T_1 L_1}{G_1 I_{p1}} = \frac{T_2 L_2}{G_2 I_{p2}} \rightarrow (4)$$

$$\frac{T_1 L_1}{G_1 I_{p1}} = -\frac{T_3 L_3}{G_3 I_{p3}} \rightarrow (5)$$

Solve for T_1, T_2, T_3 using (1), (4) and (5)

$$I_{p1} = \frac{\pi d_1^4}{32} = 7.952 \times 10^{-8} \text{ m}^4$$

$$I_{p2} = \frac{\pi (d_{2o}^4 - d_{2i}^4)}{32} = 3.623 \times 10^{-7} \text{ m}^4$$

$$I_{p3} = \frac{\pi d_3^4}{32} = 1.473 \times 10^{-7} \text{ m}^4$$

Substituting the given values of L, G and I_p into (4) and (5) we get:

$$2.278 T_1 = T_2$$

$$-5.557 T_1 = T_3$$

Substituting into (1)

$$T_1 + 2.278 T_1 + 5.557 T_1 = T_B$$

$$T_1 = 11.319 \text{ N}\cdot\text{m}$$

$$T_2 = 25.785 \text{ N}\cdot\text{m}$$

$$T_3 = -62.9 \text{ N}\cdot\text{m}$$

(b) τ_{\max} is at the outer surface of all rods.

$$\tau_{\max(1)} = \frac{T_1 (d_1/2)}{I_{p1}}$$

$$\tau_{\max(2)} = \frac{T_2 (d_2/2)}{I_{p2}}$$

$$\tau_{\max(3)} = \frac{T_3 (d_3/2)}{I_{p3}}$$

$$\tau_{\max(1)} = 2.135 \text{ MPa}$$

$$\tau_{\max(2)} = 1.779 \text{ MPa}$$

$$\tau_{\max(3)} = 7.473 \text{ MPa}$$

$$(c) \phi_B = \Delta\phi_1 = \frac{T_1 L_1}{G \cdot I_{p1}}$$

$$\phi_B = 0.01423 \text{ rad}$$

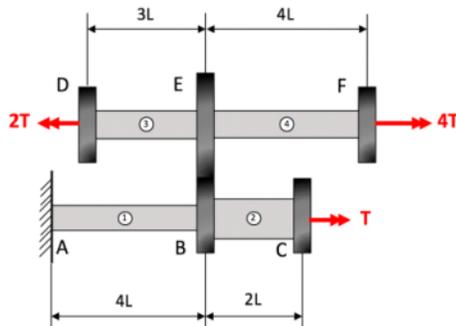
Problem 3.

The gear shaft system consists of two parallel shafts, ABC and DEF. The shafts are interconnected by gears at B and E. The diameters of members 1, 2, 3, and 4 are d_1, d_2, d_3 and d_4 , respectively. Both shafts have the same shear modulus G . Determine the angle of twist at C and F

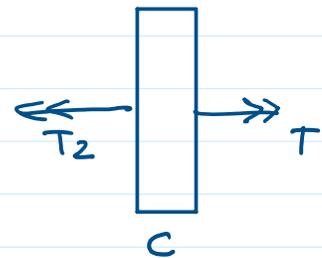
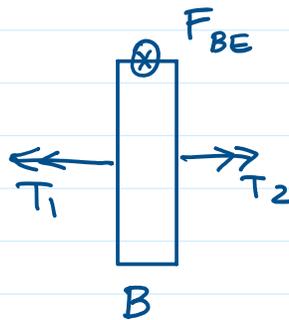
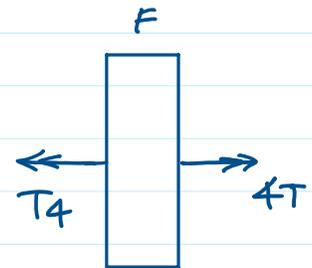
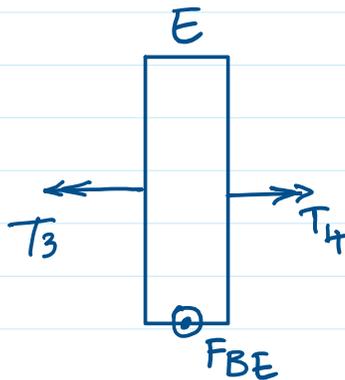
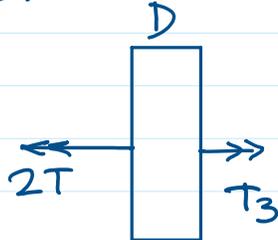
Given : $d_1 = D, d_2 = 2D, d_3 = 1.5D, d_4 = 1.5D$,

$d_B = 4D, d_E = 6D; D = 20 \text{ mm}$,

$L = 500 \text{ mm}, G = 100 \text{ GPa}, T = 1500 \text{ N m}$



FBD:



At connector D:

$$\sum T : T_3 = 2T \quad \rightarrow \textcircled{1}$$

At connector F:

$$\sum T : T_4 = 4T \quad \rightarrow \textcircled{2}$$

At gear E:

$$\sum T: T_4 = d_E F_{BE} + T_3$$

substituting (1) and (2)

$$F_{BE} = \frac{2T}{d_E} = \frac{T}{3D} \rightarrow (3)$$

At connector C:

$$\sum T: T_2 = T \rightarrow (4)$$

At gear B:

$$T_1 + d_B F_{BE} = T_2$$

$$T_1 = T - \frac{T}{3D} \cdot d_B$$

$$T_1 = -\frac{T}{3} \rightarrow (5)$$

Angle of twist of (1)

$$\Delta\phi_1 = \frac{T_1 L_1}{G I_{p1}} = \frac{-T \cdot 4L}{3 \cdot G \cdot \frac{\pi D^4}{32}}$$

$$\Delta\phi_1 = -0.637 \text{ rad}$$

Angle of twist of (2):

$$\Delta\phi_2 = \frac{T_2 L_2}{G I_{p2}} = \frac{2TL}{G \frac{\pi (2D)^4}{32}}$$

$$\Delta\phi_2 = 0.06 \text{ rad}$$

Angle of twist of (4):

$$\Delta\phi_4 = \frac{T_4 L_4}{G I_{P4}} = \frac{16 T L}{G \cdot \frac{\pi (1.5D)^4}{32}}$$

$$\Delta\phi_4 = 1.509 \text{ rad}$$

Angle of twist at C:

$$\Delta\phi_C = \Delta\phi_1 + \Delta\phi_2$$

$$\Delta\phi_C = -0.577 \text{ rad}$$

Angle of twist at F:

$$\Delta\phi_F = \Delta\phi_E + \Delta\phi_4$$

$$= -\frac{d_B}{d_E} \Delta\phi_1 + \Delta\phi_4$$

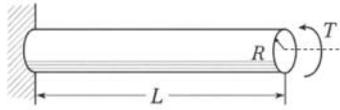
$$\Delta\phi_F = 1.934 \text{ rad}$$

Problem 9.

Consider a circular shaft of radius R , length L , and shear modulus G , subjected to torque T at the free end, as shown in the figure. Determine the effect the following changes would have:

4.1 Increasing the shaft radius, R , would _____ the maximum shear stress

- (a) Increase
- (b) Decrease
- (c) Not change



$$\tau_{max} = \frac{TR}{J_p} = \frac{2T}{\pi R^3}$$

4.2 Increasing the shaft length, L , would _____ the maximum shear stress

- (a) Increase
- (b) Decrease
- (c) Not change

Independent of L

4.3 Increasing the shaft shear modulus, G , would _____ the maximum shear stress

- (a) Increase
- (b) Decrease
- (c) Not change

Ind. of G

4.4 Increasing the shaft radius, R , would _____ the angle of rotation at the free end

- (a) Increase
- (b) Decrease
- (c) Not change

$$\Delta\phi = \frac{TL}{GI_p} = \frac{2TL}{9\pi R^4}$$

4.5 Increasing the shaft length, L , would _____ the angle of rotation at the free end

- (a) Increase
- (b) Decrease
- (c) Not change