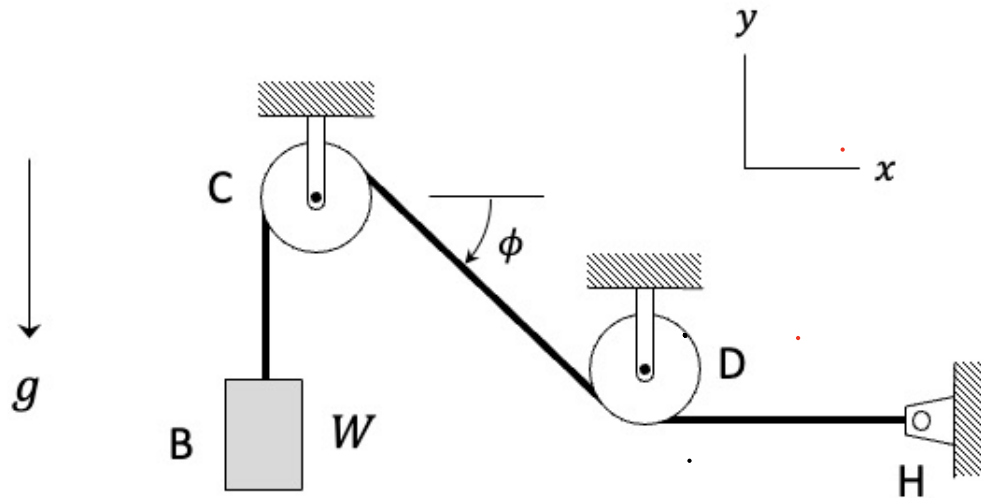


The wire-pulley system shown supports block B of weight W . The diameters of the double-sided pulley pins C and D are d_C and d_D , respectively. The diameter of the wire is d_w . The pulley pins and wire are manufactured from the same grade of steel having a tensile yield strength of σ_Y and a shear strength in yielding of τ_Y . The minimum design factors of safety for the pins and the wire are FS_{pin} , and FS_{cable} , respectively. The weight of the wire can be neglected compared to that of the block. The pulleys are to be considered to be ideal.

- Determine the diameters of the pulley pins that satisfy their design factor of safety.
- Determine the diameter of the wire that satisfies its design factor of safety.

Use the following parameter values in your analysis: $\phi = 36.87^\circ$, $W = 2 \text{ kN}$, $\sigma_Y = 220 \text{ MPa}$, $\tau_Y = 0.5\sigma_Y$, $FS_{pin} = 4$ and $FS_{wire} = 3$. Please substitute in these numerical values in the last step of your work.



FBD of pulleys

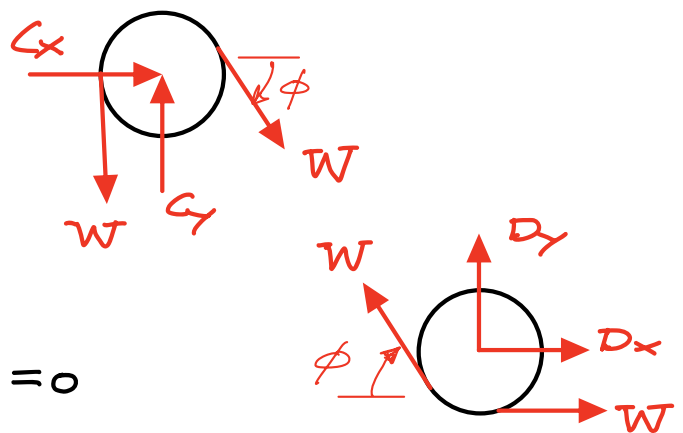
Since pulleys are ideal, the tension in cable is a constant value of WT throughout.

Equilibrium of pulleys

$$\begin{aligned}
 C: \quad \sum F_x &= C_x + W \cos \phi = 0 \\
 &\hookrightarrow C_x = -W \cos \phi \\
 \sum F_y &= -W + C_y - W \sin \phi = 0 \\
 &\hookrightarrow C_y = W(1 + \sin \phi)
 \end{aligned}$$

$$\therefore |\vec{C}| = \sqrt{C_x^2 + C_y^2} = \sqrt{(W \cos \phi)^2 + W^2(1 + \sin \phi)^2}$$

$$= W \sqrt{\cos^2 \phi + 1 + 2 \sin \phi + \sin^2 \phi}$$



$$= \sqrt{2} W \sqrt{1 + \sin \phi}$$

$$V_c = \text{Shear force in pin C} = \frac{|\vec{C}|}{2}$$

$$\tau_c = \text{shear stress in pin C} = \frac{V_c}{A_c} = \frac{|\vec{C}|}{2\pi(d_c/2)^2} = \frac{2}{\pi} \frac{|\vec{C}|}{d_c^2}$$

$$D: \sum F_x = D_x - W \cos \phi + W = 0$$

$$\hookrightarrow D_x = W(-1 + \cos \phi)$$

$$\sum F_y = D_y + W \sin \phi = 0$$

$$\hookrightarrow D_y = -W \sin \phi$$

$$\begin{aligned} \therefore |\vec{D}| &= \sqrt{D_x^2 + D_y^2} = \sqrt{W^2(-1 + \cos \phi)^2 + (-W \sin \phi)^2} \\ &= W \sqrt{1 - 2\cos \phi + \cos^2 \phi + \sin^2 \phi} \\ &= \sqrt{2} W \sqrt{1 - \cos \phi} \end{aligned}$$

$$\tau_D = \text{shear stress in pin D} = \frac{2}{\pi} \frac{|\vec{D}|}{d_D^2}$$

$$(a) \text{ For } \phi = 36.87^\circ$$

$$|\vec{C}| = \sqrt{2} W \sqrt{1 + 0.6} = \sqrt{3.2} W$$

$$|\vec{D}| = \sqrt{2} W \sqrt{1 - 0.8} = \sqrt{0.8} W$$

$$\therefore \begin{cases} \tau_c = \frac{|\vec{C}|/2}{\pi(d_c/2)^2} = \frac{2|\vec{C}|}{\pi d_c^2} \\ \tau_D = \frac{|\vec{D}|/2}{\pi(d_D/2)^2} = \frac{2|\vec{D}|}{\pi d_D^2} \end{cases}$$

$$\text{and } FS_c = \frac{\tau_Y}{\tau_c} = \frac{\pi d_c^2}{2|\vec{C}|} \tau_Y$$

$$\hookrightarrow d_c = \sqrt{\frac{2 FS_c |\vec{C}|}{\pi \tau_Y}} = \sqrt{\frac{(2)(FS_c) \sqrt{3.2} W}{\pi \tau_Y}} \quad \leftarrow d_c$$

$$FS_D = \frac{\tau_Y}{\tau_D} = \frac{\pi d_D^2}{2|\vec{D}|} \tau_Y$$

$$\hookrightarrow d_D = \sqrt{\frac{(2)(FS_D) \sqrt{0.8} W}{\pi \tau_Y}} \quad \leftarrow d_D$$

$$b) \sigma_w = \frac{W}{A_w} = \frac{W}{\pi(dw/2)^2} = \frac{4W}{\pi dw^2}$$

$$\Rightarrow FS_w = \frac{\sigma_Y}{\sigma_w} = \frac{\pi dw^2}{4W} \sigma_Y \Rightarrow dw = \sqrt{\frac{4W(FS_w)}{\pi \sigma_Y}} \quad \leftarrow dw$$