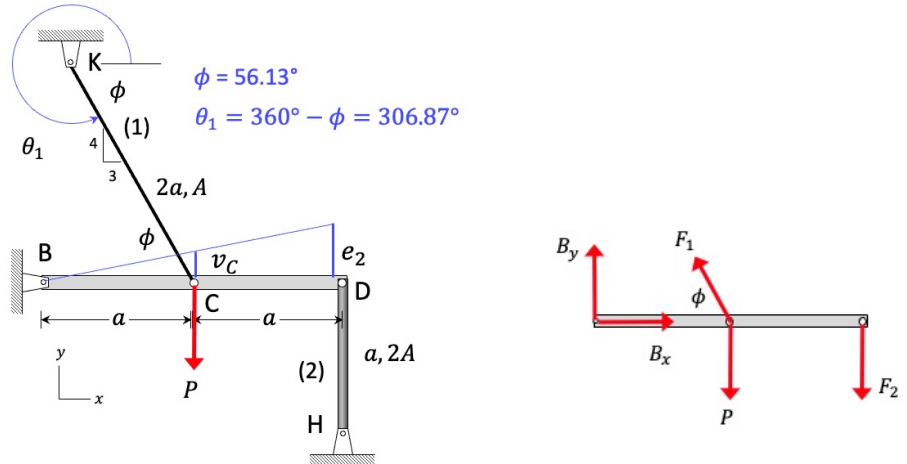


Problem No. 1 – 20 pts

Elements (1) and (2) have lengths of $2a$ and a , respectively, cross-sectional areas of A and $2A$, respectively, and identical Young's moduli E . The elements are pinned to the rigid bar BD as shown in the figure. A force P acts at pin C on BD. Determine the load (force) carried by elements (1) and (2). *You are asked to clearly label the four steps in your solution.*



1. Equilibrium

$$(1) \sum M_B = -Pa - F_2(2a) + (F_1 \sin \phi)a = 0 \Rightarrow \frac{4}{5}F_1 - 2F_2 = P$$

2. Load/deformation

$$(2) e_1 = \frac{F_1(2a)}{EA}$$

$$(3) e_2 = \frac{F_2 a}{E(2A)}$$

3. Compatibility

$$e_2 = 2v_C ; \text{ similar triangles}$$

$$e_1 = u_C \cos \theta_1 + v_C \sin \theta_1 = \frac{3}{5}u_C - \frac{4}{5}v_C$$

$$u_C = 0$$

Therefore:

$$(4) e_1 = -\frac{2}{5}e_2$$

4. Solve

Combining (2)-(4):

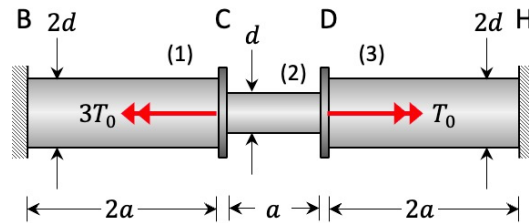
$$\frac{2F_1 a}{EA} = -\frac{2}{5} \left(\frac{F_2 a}{2EA} \right) \Rightarrow F_2 = -10F_1$$

Substituting into (1):

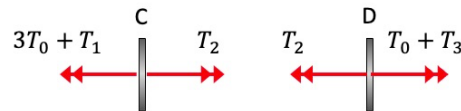
$$\frac{4}{5}F_1 - 2(-10F_1) = P \Rightarrow F_1 = \frac{5}{104}P \Rightarrow F_2 = -\frac{50}{104}P$$

Problem No. 2 – 20 pts

The shaft shown is made up of three elements having solid circular cross-sections, each of a material having a shear modulus of G . Determine the torque carried by each element. *You are asked to clearly label the four steps in your solution.*



1. Equilibrium



- (1) Connector C: $\Sigma M = -3T_0 - T_1 + T_2 = 0 \Rightarrow T_1 = T_2 - 3T_0$
 (2) Connector D: $\Sigma M = T_0 - T_2 + T_3 = 0 \Rightarrow T_3 = T_2 - T_0$

2. Torque/rotation angle

- (3) $\Delta\phi_1 = \frac{T_1(2a)}{GI_{P1}}$ where $I_{P1} = \frac{\pi}{2} \left(\frac{2d}{2}\right)^4 = \frac{\pi}{2} d^4$
 (4) $\Delta\phi_2 = \frac{T_2(a)}{GI_{P2}}$ where $I_{P2} = \frac{\pi}{2} \left(\frac{d}{2}\right)^4 = \frac{\pi}{32} d^4$
 (5) $\Delta\phi_3 = \frac{T_3(2a)}{GI_{P3}}$ where $I_{P3} = \frac{\pi}{2} \left(\frac{2d}{2}\right)^4 = \frac{\pi}{2} d^4$

3. Compatibility

- $\phi_C = \phi_B + \Delta\phi_1 = \Delta\phi_1$
 $\phi_D = \phi_C + \Delta\phi_2 = \Delta\phi_1 + \Delta\phi_2$
 (6) $\phi_H = \phi_D + \Delta\phi_3 = \Delta\phi_1 + \Delta\phi_2 + \Delta\phi_3 = 0$

4. Solve

$$(3)-(6) \Rightarrow \frac{4 T_1 a}{\pi G d^4} + \frac{32 T_2 a}{\pi G d^4} + \frac{4 T_3 a}{\pi G d^4} = 0 \Rightarrow T_1 + 8T_2 + T_3 = 0$$

Combining with equations (1) and (2):

$$T_2 - 3T_0 + 8T_2 + T_2 - T_0 = 0 \Rightarrow T_2 = \frac{2}{5} T_0$$

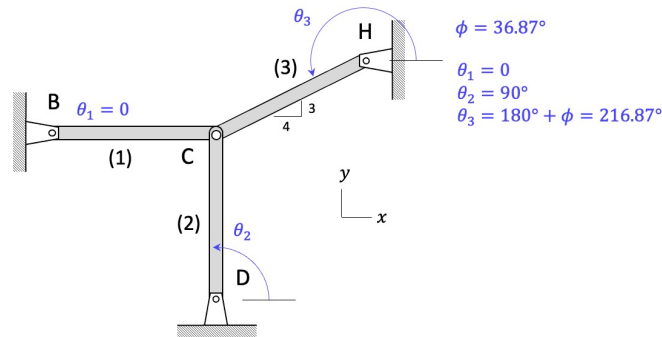
Also:

$$T_1 = T_2 - 3T_0 = -\frac{13}{5} T_0$$

$$T_3 = T_2 - T_0 = -\frac{3}{5} T_0$$

Problem No. 3 – 20 pts

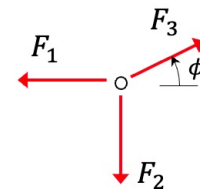
The truss shown is made up of three identical members, each has a Young's modulus of E , a cross-sectional area A , a length of a and thermal coefficient of expansion of α . The temperature of members (1) and (3) is each increased by an amount of ΔT , with the temperature of (2) remaining unchanged. Find the load (force) carried by each member, and state whether the member is in tension or compression. *You are asked to clearly label the four steps in your solution. You must also clearly state the member angles for each member used in Step 3.*



1. Equilibrium

$$(1) \Sigma F_x = F_3 \cos \phi - F_1 = 0 \Rightarrow F_1 = \frac{4}{5} F_3$$

$$(2) \Sigma F_y = F_3 \sin \phi - F_2 = 0 \Rightarrow F_2 = \frac{3}{5} F_3$$



2. Load/deformation

$$(3) e_1 = \frac{F_1 a}{EA} + \alpha \Delta T a$$

$$(4) e_2 = \frac{F_2 a}{EA}$$

$$(5) e_3 = \frac{F_3 a}{EA} + \alpha \Delta T a$$

3. Compatibility

$$(6) e_1 = u_C \cos \theta_1 + v_C \sin \theta_1 = u_C$$

$$(7) e_2 = u_C \cos \theta_2 + v_C \sin \theta_2 = v_C$$

$$(8) e_3 = u_C \cos \theta_3 + v_C \sin \theta_3 = -\frac{4}{5} u_C - \frac{3}{5} v_C$$

4. Solve

Using (3)-(8):

$$e_3 = -\frac{4}{5} e_1 - \frac{3}{5} e_2 \Rightarrow 5 \left(\frac{F_3 a}{EA} + \alpha \Delta T a \right) = -4 \left(\frac{F_1 a}{EA} + \alpha \Delta T a \right) - 3 \left(\frac{F_2 a}{EA} \right) \Rightarrow$$

$$4F_1 + 3F_2 + 5F_3 = -9\alpha \Delta T EA$$

Combining with (1) and (2):

$$4 \left(\frac{4}{5} F_3 \right) + 3 \left(\frac{3}{5} F_3 \right) + 5F_3 = -9\alpha \Delta T EA \Rightarrow F_3 = -\frac{9}{10} \alpha \Delta T EA \text{ (compression)}$$

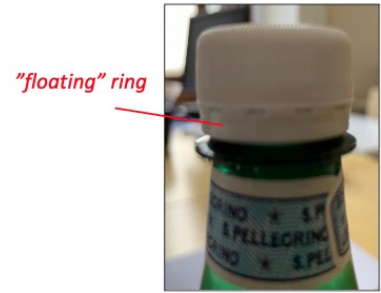
$$(1) \Rightarrow F_1 = -\frac{18}{25} \alpha \Delta T EA \text{ (compression)}$$

$$(2) \Rightarrow F_2 = -\frac{27}{50} \alpha \Delta T EA \text{ (compression)}$$

Problem No. 4

PART 4.A – 3 points

Suppose you open a twist-off cap on a water bottle for which the cap has a floating ring. In opening the bottle, does the cap fail due to *normal stress* or *shear stress*? Provide a brief explanation.

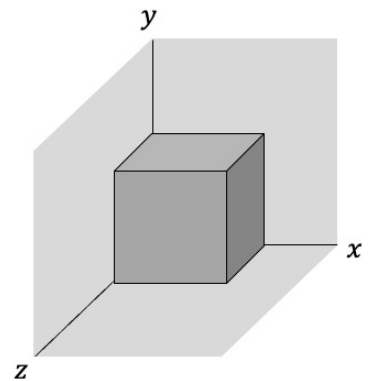


Before opening

As discussed in lecture, twisting on the cap produce a thrust force on the cap from the bottle threads. This produces normal stresses in the tabs connecting the cap to the floating ring.

PART 4.B – 3 points

A uniform block made up of a material with a Young’s modulus E and Poisson’s ratio rests in a rigid, smooth corner. Uniform *compressive* stresses of σ_0 and $3\sigma_0$ act on the xz -faces of the block, respectively, with the y -face left stress-free. Determine the *three components of strain* experienced by the block. Consider the weight of the block to be negligible.



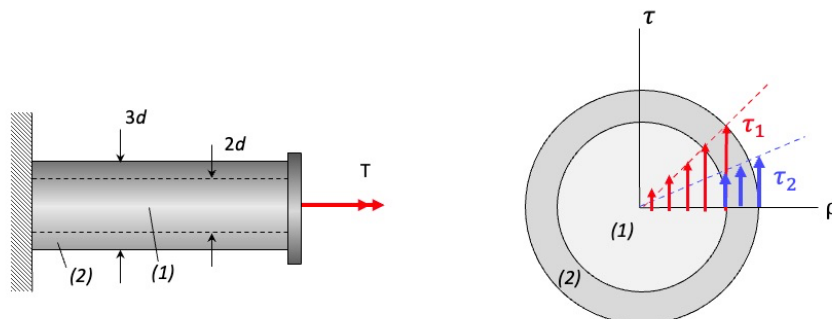
$$\epsilon_x = \frac{1}{E} [-\sigma_0 - \nu(0 - 3\sigma_0)] = \frac{\sigma_0}{E} (-1 + 3\nu)$$

$$\epsilon_y = \frac{1}{E} [0 - \nu(-\sigma_0 - 3\sigma_0)] = \frac{\sigma_0}{E} (4\nu)$$

$$\epsilon_z = \frac{1}{E} [-3\sigma_0 - \nu(-\sigma_0 + 0)] = \frac{\sigma_0}{E} (-3 + \nu)$$

PART 4.C – 4 points

A composite shaft is made up of an outer shell (2) and an inner core (1). The shear moduli for (1) and (2) are known to be $2G$ and G , respectively. On the figure of the cross-section below, make a sketch of the distribution of shear stress τ vs. the radial position ρ on the cross-section of the composite shaft. Show the location of the maximum shear stress on the cross-section.

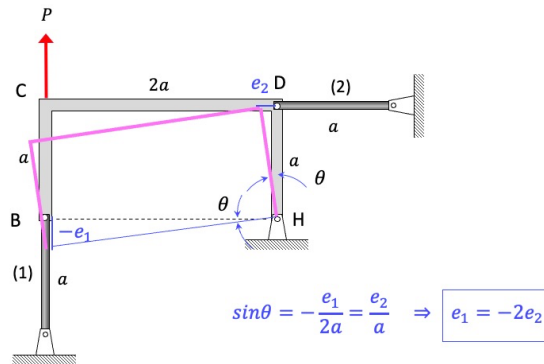


If the shear strain is written as: $\gamma = m\rho$ then: $\tau_1 = 2mG\rho$ and $\tau_2 = mG\rho$.
Therefore, $\tau_{1,max} = 2mGd$ and $\tau_{2,max} = 3mG/2$.

Problem No. 4 (continued)

PART 4.D – 4 points

Rigid frame member BCDH is supported by elastic members (1) and (2). A force P acts at location C on frame member BCDH. Let e_1 and e_2 represent the elongation of members (1) and (2), respectively. Determine the compatibility equation relating e_1 and e_2 .



PART 4.E – 6 points

Draw the shear force/bending moment diagrams for the simply-supported beam shown below.

$$\Sigma M_D = -B_y(2a) + p_0a(a/2) - p_0a(3a/2) = 0 \Rightarrow B_y = -p_0a / 2$$

$$\Sigma F_y = B_y + D_y + p_0a - p_0a = 0 \Rightarrow D_y = -B_y = p_0a / 2$$

$$V(a) = V(0) + p_0a = -p_0a/2 + p_0a = p_0a/2$$

$$V(2a) = V(a) - p_0a = p_0a/2 - p_0a = -p_0a / 2$$

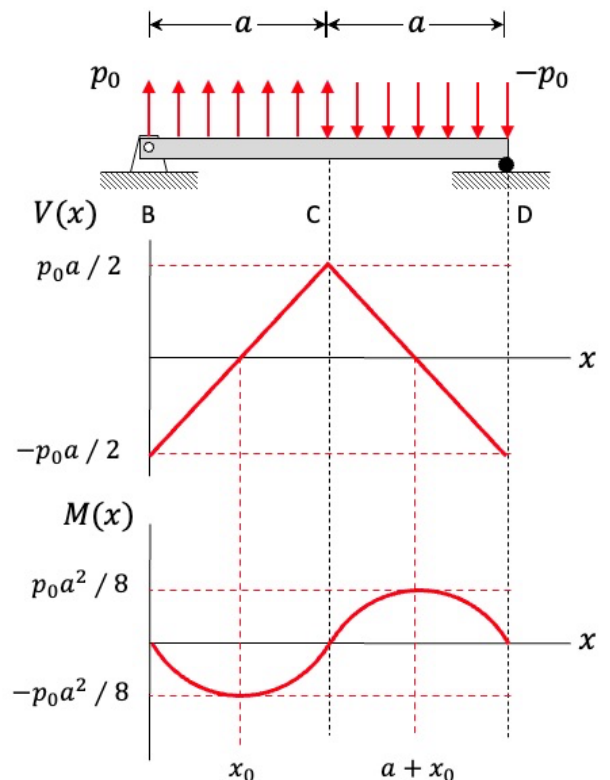
$$x_0 = a / 2$$

$$M(x_0) = M(0) - (p_0a / 2)x_0 / 2 = -p_0a^2 / 8$$

$$M(a) = M(x_0) + p_0a^2 / 8 = 0$$

$$M(a + x_0) = M(a) + p_0a^2 / 8 = p_0a^2 / 8$$

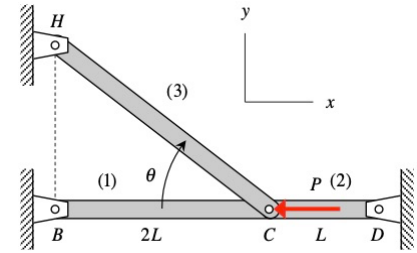
$$M(2a) = M(a) - p_0a^2 / 8 = 0$$



Problem No. 5

PART 5.A – 4 points

The truss shown is made up of truss elements (1), (2) and (3). A horizontal force P is applied to Joint C. Let σ_3 represent the stress developed in element (3). Circle the correct response. Provide a short explanation.

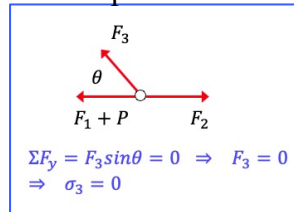


a) $\sigma_3 > 0$ (tension)

b) $\sigma_3 = 0$

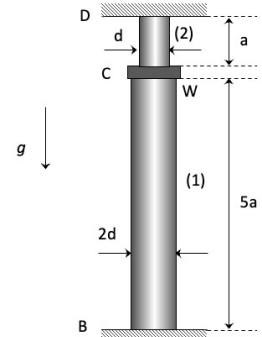
c) $\sigma_3 < 0$ (compression)

d) More information is needed in order to answer this question.



PART 5.B – 4 points

Rod elements (1) and (2) have circular solid cross-sections, and are made of the same material having a Young's modulus of E . Rigid connector C has a weight of W , whereas the weights of the rod elements are negligible. Let F_1 and F_2 be the axial loads carried by (1) and (2), respectively. Choose the correct response below. Provide a short explanation.



a) $|F_1| > |F_2|$

b) $|F_1| = |F_2|$

c) $|F_1| < |F_2|$

d) More information is needed in order to answer this question.

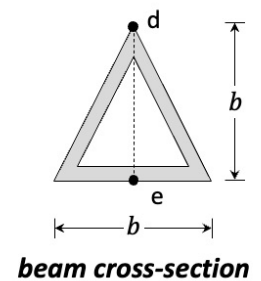
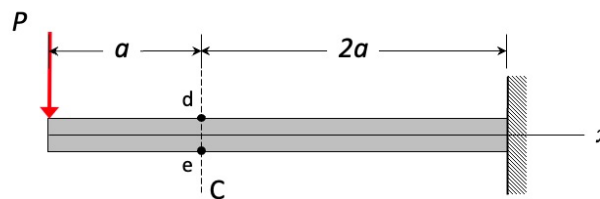
$$|e_1| = \frac{|F_1|(5a)}{E\pi(2d/2)^2} = \frac{5|F_1|a}{\pi Ed^2}$$

$$|e_2| = \frac{|F_2|(a)}{E\pi(d/2)^2} = \frac{4|F_2|a}{\pi Ed^2}$$

$$|e_1| = |e_2| \Rightarrow |F_1| = \frac{4}{5}|F_2|$$

PART 5.C – 4 points

Consider the end-loaded cantilevered beam shown that has a triangular-shaped tubular cross-section of uniform wall thickness. Let σ_d and σ_e be the normal stresses at points "d" and "e" on the cross-section at C, respectively. Choose the correct response below. Provide a short justification.



a) $|\sigma_d| > |\sigma_e|$

b) $|\sigma_d| = |\sigma_e|$

c) $|\sigma_d| < |\sigma_e|$

d) More information is needed in order to answer this question.

"d" is further away from the neutral axis (centroid) than is "e". Therefore, the magnitude of the normal stress at "d" is greater.

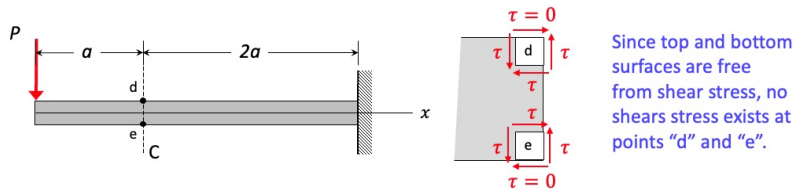
Problem No. 5 (continued)

PART 5.D – 4 points

Same cantilevered beam as Part 5.C, except here the shape of the beam cross-section is *unknown*. Choose the correct *TRUE/FALSE* response below. Provide a short justification.

TRUE **FALSE**: Shear stress at “d” and “e” is zero, for any cross-section shape.

HINT: Consider the stress elements at “d” and “e”.



PART 5.E – 4 points

Again, the same cantilevered beam as Part 5.C, except here the beam has the rectangular cross-section shown. Let τ_p and τ_q represent the shear stress on the beam cross-section at points “p” and “q”. Choose the correct response below. Provide a short justification.

a) $|\tau_p| > |\tau_q|$

b) $|\tau_p| = |\tau_q|$

c) $|\tau_p| < |\tau_q|$

d) More information is needed in order to answer this question.

Here the maximum shear stress occurs at the neutral axis. Point “p” is closer to the neutral axis than is “q”; therefore, its shear stress has a larger magnitude.

