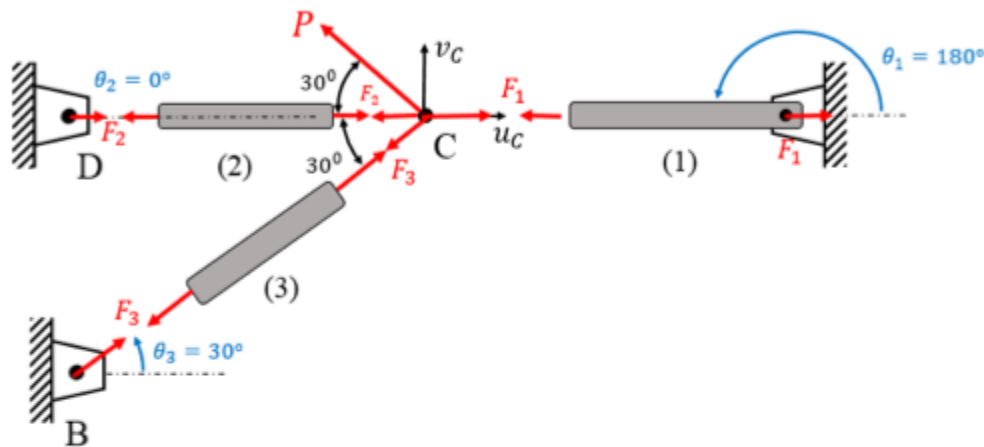


Problem 1

- a. The angular orientations of members (1), (2), and (3) w.r.t pinned ends H, D, and B are

$$\theta_1 = 180^\circ, \theta_2 = 0^\circ, \theta_3 = 30^\circ.$$



From the free body diagram of joint C,

$$\Sigma F_x = F_1 - F_2 - F_3 \cos 30^\circ - P \cos 30^\circ = 0$$

$$\Sigma F_y = F_3 \sin 30^\circ - P \sin 30^\circ = 0$$

Static equilibrium analysis of joint yields 2 equations and three unknowns F_1, F_2, F_3 . It means that the problem is indeterminate and needs compatibility conditions to solve for the unknowns.

b. Elongation:

$$e_1 = \frac{F_1(6L)}{(2A)E} = \frac{3F_1L}{EA}; \quad e_2 = \frac{F_2(4L)}{A(2E)} = \frac{2F_2L}{EA}; \quad e_3 = \frac{F_3(2L)}{E(2A)} = \frac{F_3L}{EA}$$

c. Compatibility:

$$\begin{aligned} e_1 &= u_C \cos \theta_1 + v_C \sin \theta_1 \\ \Rightarrow \frac{3F_1L}{EA} &= u_C \cos 180^\circ + v_C \sin 180^\circ \Rightarrow \frac{3F_1L}{EA} = -u_C \\ e_2 &= u_C \cos \theta_2 + v_C \sin \theta_2 \\ \Rightarrow \frac{2F_2L}{EA} &= u_C \cos 0^\circ + v_C \sin 0^\circ \Rightarrow \frac{2F_2L}{EA} = u_C \end{aligned}$$

$$e_3 = u_c \cos \theta_3 + v_c \sin \theta_3$$

$$\Rightarrow \frac{F_3 L}{EA} = u_c \cos 30^\circ + v_c \sin 30^\circ \Rightarrow \frac{F_3 L}{EA} = \frac{\sqrt{3}}{2} u_c + \frac{1}{2} v_c$$

d. From previous equations

$$\begin{aligned} \frac{3F_1 L}{EA} &= -\frac{2F_2 L}{EA} \\ \Rightarrow F_2 &= \frac{-3}{2} F_1 \end{aligned}$$

From the equilibrium equations,

$$F_3 = P$$

and

$$F_1 + \frac{3}{2} F_1 - P \cos 30^\circ - P \cos 30^\circ = 0$$

$$\Rightarrow F_1 = \frac{2\sqrt{3}}{5} P$$

$$\Rightarrow F_2 = \frac{-3}{2} F_1 = \frac{-3\sqrt{3}}{5} P$$

$$u_c = \frac{2F_2 L}{EA} = \frac{-6\sqrt{3} PL}{5 EA}$$

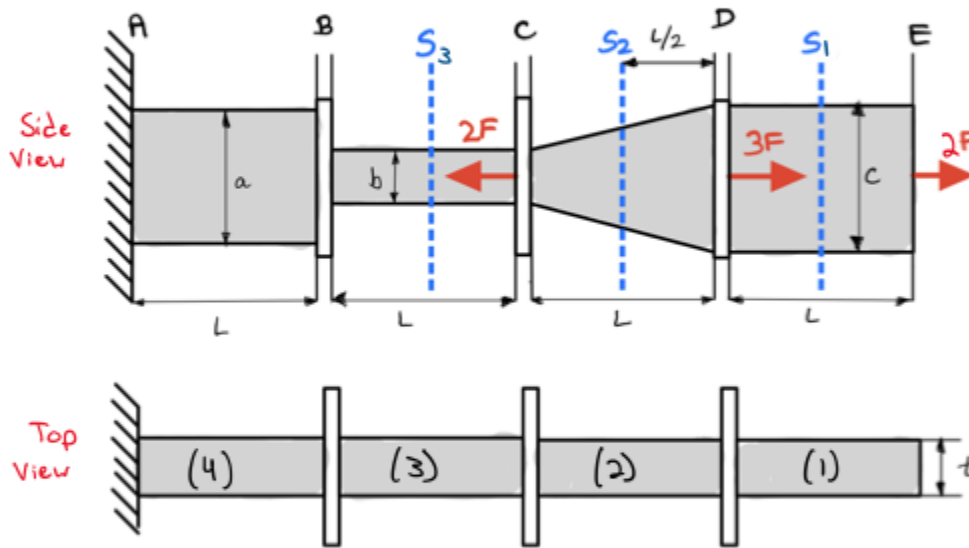
$$\frac{F_3 L}{EA} = \frac{\sqrt{3}}{2} u_c + \frac{1}{2} v_c \Rightarrow \frac{PL}{EA} - \frac{\sqrt{3}}{2} \left(\frac{-6\sqrt{3} PL}{5 EA} \right) = \frac{1}{2} v_c$$

$$\Rightarrow v_c = \frac{28 PL}{5 EA}$$

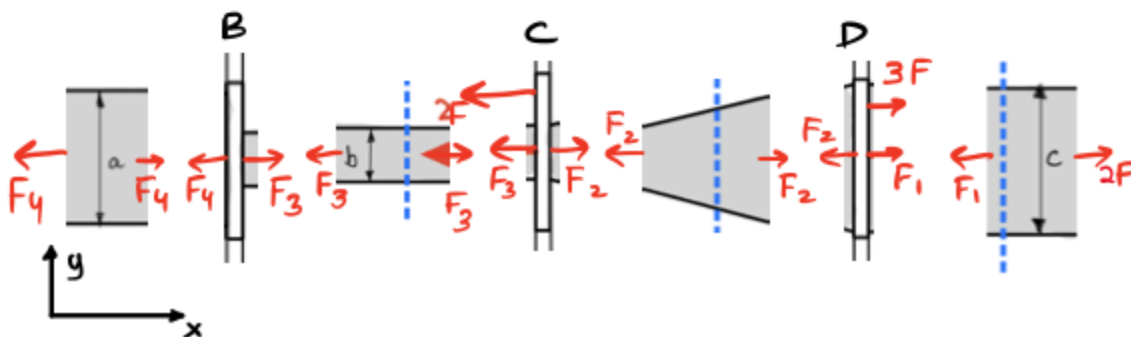
Problem 3.2 (10 points)

The axial bar shown in Fig.1 has four sections. Each section is connected to the neighbouring sections by rigid connectors (at B, C and D). The size of the rigid connectors is negligible. The first section AB, second section BC and the last section DE have uniform rectangular cross sections with width a , b and c respectively. The section CD has width varying linearly from b to c . The length of each section is L . All the sections have same thickness t . Three loads F , $3F$ and $2F$ are applied to the bar as shown in the figure. Assume the Young's Modulus of all the sections is E .

- (a) Find expressions for stresses at sections S_1 , S_2 and S_3 . (S_2 is midway of section CD as shown)
- (b) Find expressions for displacement at points B and C



Free body Diagram :



Now,

$$\text{At connector B: } \rightarrow \sum F_x = 0: F_3 - F_4 = 0$$

$$F_4 = F_3$$

$$\text{connector C: } \rightarrow \sum F_x = 0: F_2 - F_3 - 2F = 0$$

$$F_3 = F_2 - 2F$$

$$\text{connector D: } \rightarrow \sum F_x = 0: F_1 + 3F - F_2 = 0$$

$$F_2 = F_1 + 3F$$

But looking at Section S_3 , we know that

$$F_1 = 2F$$

$$\therefore F_2 = 5F, F_3 = 3F \text{ and } F_4 = 3F$$

(a) Stresses:

$$\sigma_{S_3} = \frac{F_3}{A_3} = \frac{3F}{b \times t}$$

$$\sigma_{S_2} = \frac{F_2}{A_2} = \frac{5F}{\left(\frac{b+c}{2}\right)t} = \frac{10F}{(b+c)t}$$

$$\sigma_{S_1} = \frac{F_1}{A_1} = \frac{2F}{c \times t}$$

$$b + \frac{c-b}{L} \cdot x = a' + b'x$$

$$\frac{SF}{E} \int \frac{dx}{A(x)} = \frac{SF}{Et} \int \frac{dx}{a'+b'x}$$

$$\frac{SF}{Et} \left[\frac{1}{b'} (\ln(b'+a') - \ln(a)) \right]$$

$$\frac{SF}{Et} \left[\frac{L}{c-b} (\ln(c+b) - \ln(b)) \right]$$

$$\frac{SFL}{Et(c-b)} \left(\ln \frac{c}{b} \right)$$

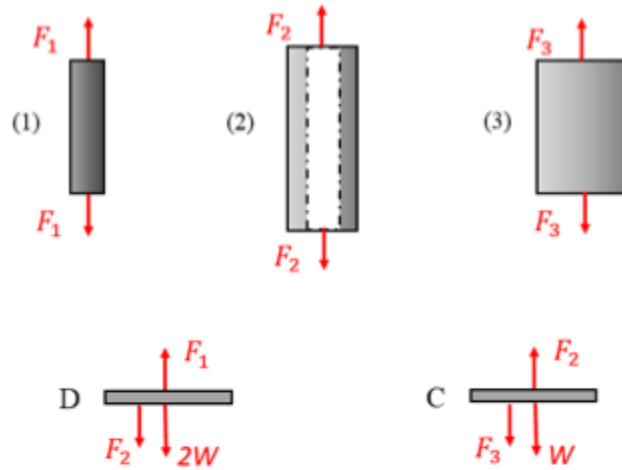
$$(b) u_B = u_{AB} + u_A = \frac{F_4(L_{AB})}{A_4 E} = \frac{3F \cdot L}{(at)E}$$

$$u_c = u_B + u_{BC} = \frac{3FL}{atE} + \frac{3FL}{btE}$$

$$u_d = u_c + u_{cd} = \frac{3FL}{atE} + \frac{3FL}{btE} + \frac{SFL}{Et(c-b)} \ln \left(\frac{c}{b} \right)$$

Problem 3

a) Let F_1 , F_2 and F_3 represent the tensile axial forces carried by rods (1),(2) and (3), respectively.



From the FBD above,

$$\Sigma F_D = F_1 - F_2 - 2W = 0$$

$$\Sigma F_C = F_2 - F_3 - W = 0$$

$$\Rightarrow F_2 = F_3 + W; \quad F_1 = F_2 + 2W = F_3 + 3W \text{ [FBD + Equilibrium: 3pt]}$$

Force-Elongation:

$$e_1 = \frac{F_1 L_1}{E_1 A_1} = \frac{F_1 L}{E \frac{\pi d^2}{4}} = \frac{4F_1 L}{E \pi d^2} \text{ [0.5pt]}$$

$$e_2 = \frac{F_2 L_2}{E_2 A_2} = \frac{F_2 \frac{3}{2} L}{E \frac{3\pi d^2}{4}} = \frac{2F_2 L}{E \pi d^2} \text{ [0.5pt]}$$

$$e_3 = \frac{F_3 L_3}{E_3 A_3} = \frac{F_3 L}{E \frac{9\pi d^2}{4}} = \frac{4F_3 L}{9E \pi d^2} \text{ [0.5pt]}$$

Compatibility:

$$u_B = u_H + e_1 + e_2 + e_3 = 0$$

$$\Rightarrow e_1 + e_2 + e_3 = 0 \text{ [1pt]}$$

Combine this with the equilibrium equation to get:

$$\begin{aligned} \frac{4F_1L}{E\pi d^2} + \frac{2F_2L}{E\pi d^2} + \frac{4F_3L}{9E\pi d^2} = 0 &\Rightarrow \frac{4(F_3 + 3W)L}{E\pi d^2} + \frac{2(F_3 + W)L}{E\pi d^2} + \frac{4F_3L}{9E\pi d^2} = 0 \text{ [0.5pt]} \\ &\Rightarrow F_3 = -\frac{63}{29}W \\ \Rightarrow \sigma_3 = \frac{F_3}{A_3} = \frac{-\frac{63}{29}W}{\frac{9\pi d^2}{4}} = -\frac{28W}{29\pi d^2} \text{ (in compression) [1pt]} \end{aligned}$$

b) The equilibrium equation becomes:

$$\Sigma F_D = F_1 - F_2 - 2W + P = 0$$

$$F_1 = F_2 + 2W - P = F_3 + 3W - P \text{ [1pt]}$$

Take the compatibility equation:

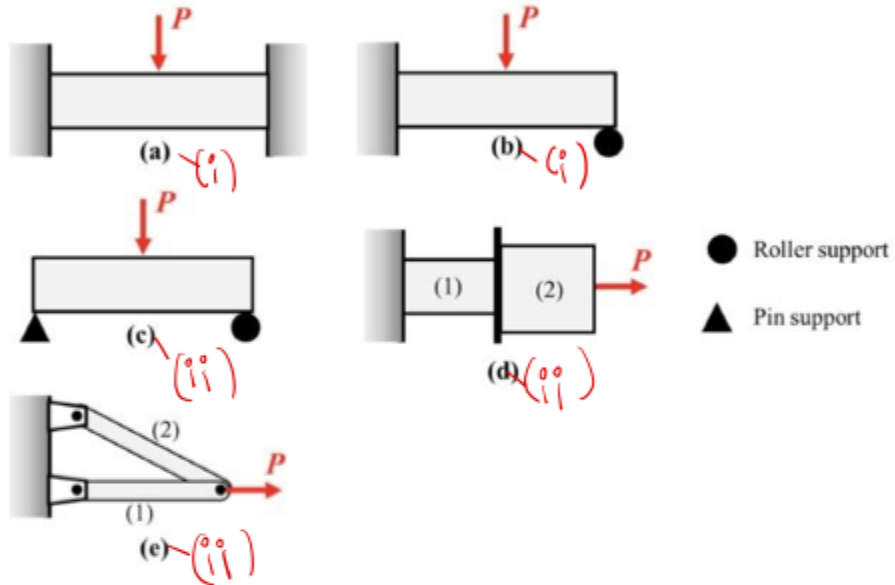
$$\begin{aligned} \frac{4F_1L}{E\pi d^2} + \frac{2F_2L}{E\pi d^2} + \frac{4F_3L}{9E\pi d^2} = 0 &\Rightarrow \frac{4(F_3 + 3W - P)L}{E\pi d^2} + \frac{2(F_3 + W)L}{E\pi d^2} + \frac{4F_3L}{9E\pi d^2} = 0 \\ &\Rightarrow F_3 = -\frac{63}{29}W + \frac{18}{29}P \\ \Rightarrow \sigma_3 = \frac{F_3}{A_3} = \frac{-\frac{63}{29}W + \frac{18}{29}P}{\frac{9\pi d^2}{4}} \text{ [1pt]} \end{aligned}$$

Since that the magnitude of the compressive stress in (3) reduced by 50% from that found in part a):

$$\begin{aligned} \frac{-\frac{63}{29}W + \frac{18}{29}P}{\frac{9\pi d^2}{4}} = 0.5 \times \frac{-\frac{63}{29}W}{\frac{9\pi d^2}{4}} \\ \Rightarrow \frac{18}{29}P = 0.5 \times \left(\frac{63}{29}W\right) \Rightarrow P = \frac{7}{4}W \text{ [1pt]} \end{aligned}$$

Problem 3.4

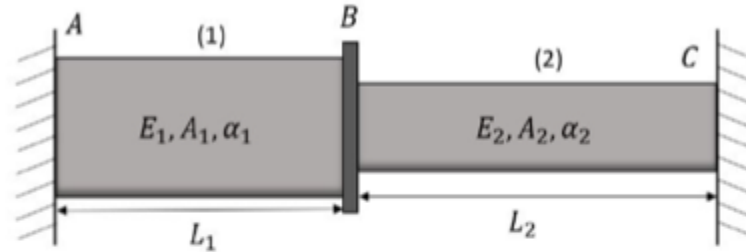
1. Match the following six structures (a)-(e) with correct option given in i-iii.



- i. Statically indeterminate structure
- ii. Statically determinate structure
- iii. Insufficient information

Number of variables vs number of equation

3. Consider a bar made of two sections fixed at both ends. For section (1) let the length be L_1 , area A_1 , Young's modulus E_1 and coefficient of thermal expansion α_1 . The corresponding values for section (2) are L_2 , A_2 , E_2 and α_2 . It is known that $L_1 < L_2$, $E_1 > E_2$, $A_1 > A_2$ and $\alpha_1 > \alpha_2$. The bar is free of stress at temperature T_1 . Let σ_1 and σ_2 represent the axial stresses in section 1 and 2, respectively, after the rise in temperature. The temperature is raised from T_1 to T_2 ($T_2 > T_1$).



If δ_1 is the change in length of section 1 and δ_2 is the change in length of section 2, which of the following statements is true?

- (a) $\delta_1 = \delta_2 = 0$
 (b) $\delta_1 + \delta_2 = 0$
 (c) $\delta_1 = \delta_2 \neq 0$
 (d) $\delta_1 = \frac{E_1}{E_2} \delta_2$

$$\delta_C = \delta_A + \delta_L + \delta_2$$

$$\delta_C = \delta_A = 0$$

(Elongation at the support should be zero)