

Problem 1 (10 points):

Dwight Schrute from *The Office US* is attempting his tightrope stunt again and wants to present a spectacle (*Figure 1.1 left*). He has modified the high-wire design in a Mechanics textbook and plans to make it taller. His design is as described in *figure 1.2*. The high-wire is attached to a rigid vertical beam AC and is kept taut by a tensioner cable BD. At C, the beam is attached by a 20 mm diameter bolt to the bracket (also shown in the figure). The tension in the wire is 7 kN. The maximum allowable shear stress in the bolt C is 31.25 MPa. As his friend, you are asked to help him figure out the maximum length L that he can consider. Assume the high-wire to be horizontal and neglect the weight of AC.

[Note: Please do not try this at home]

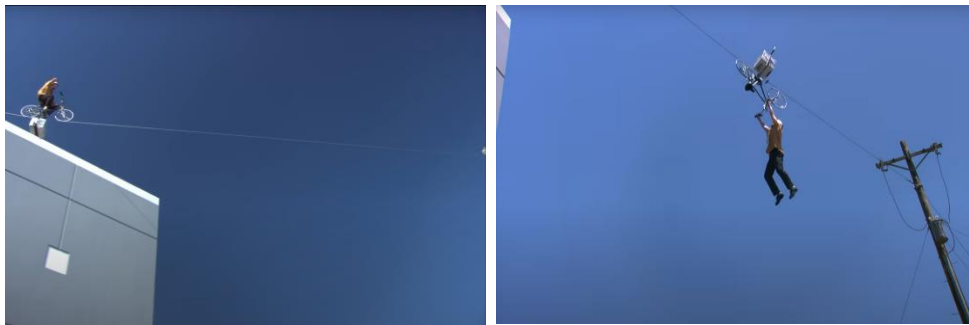


Figure 1.1: Left: Dwight's tightrope stunt; Right: His failed attempt.

[Image courtesy: PeacockTV]

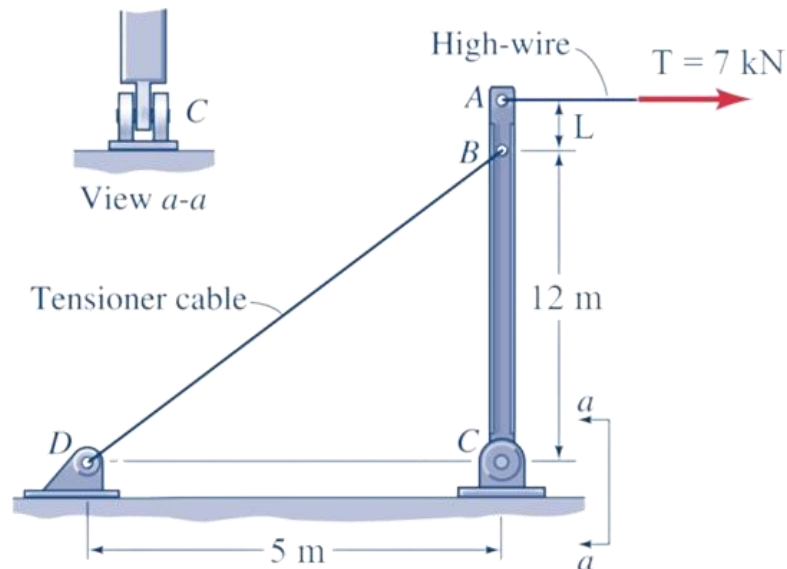
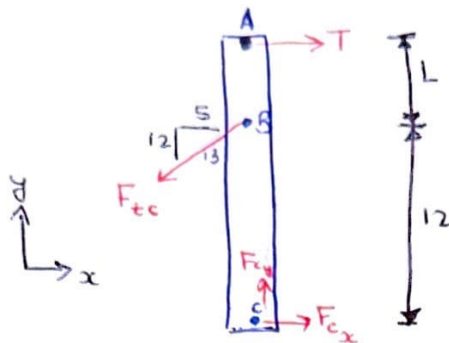


Figure 1.2: Design of the high-wire setup.

Solution 1:

FBD:



$$T = 7 \text{ kN}$$

$$\tau_{all_c} = 31.25 \text{ MPa}$$

- Sum of moments about B:

$$\sum M_B = 0 = -T(L) + F_{cx}(12) \quad (1)$$

- Sum of forces in x and y direction:

$$\sum F_x = 0 = T + F_{cx} - \frac{5}{13} F_{tc} \quad (2)$$

$$\sum F_y = 0 = F_{cy} - \frac{12}{13} F_{tc} \quad (3)$$

- Now, the bolt C is in double shear

$$\therefore A = 2 \left(\pi \frac{[0.02]^2}{4} \right) \text{ m}^2 = 6.283 \times 10^{-4} \text{ m}^2$$

$$\tau_{all_c} = \frac{F_c}{A} = \frac{\sqrt{(F_{cx})^2 + (F_{cy})^2}}{A}$$

using (2) and (3)

$$31.25 \text{ MPa} = \frac{\sqrt{\left(\frac{5}{13} F_{tc} - 7000\right)^2 + \left(\frac{12}{13} F_{tc}\right)^2}}{6.283 \times 10^{-4}}$$

$$F_{tc} = 21233 \text{ N}$$

$F_{tc} = -15848 \text{ N}$
 neglected because cable comes in Compression

using (2) $\Rightarrow F_{cx} \approx 1.17 \text{ kPa}$

using (1) $\Rightarrow L \approx 2 \text{ m}$

Problem 2 (10 points):

Links BC and DE are connected to a rigid member ACD as shown in *figure 2*. A load P is applied to the structure at A. Each pin has a diameter of 10 mm and experiences single shear. The material strength of the pins is $\tau = 250$ MPa and the material strength in tension of the links is $\sigma = 500$ MPa. Both BC and DE have a cross-sectional area of 125 mm^2 . Calculate the maximum P so that the structure does not fail.

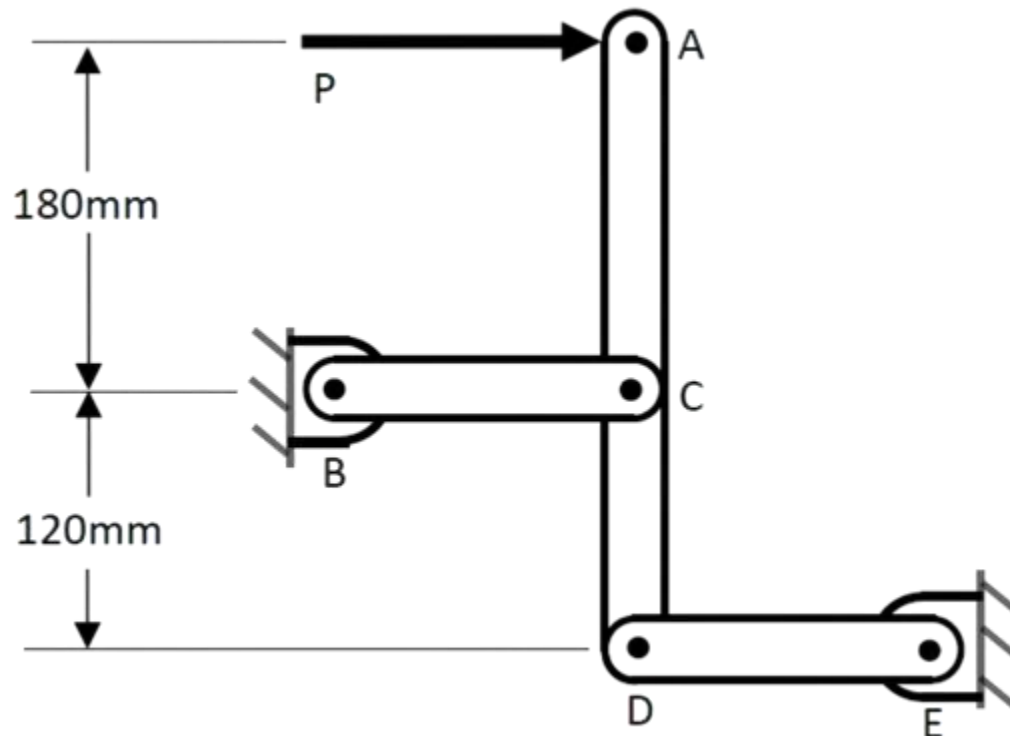
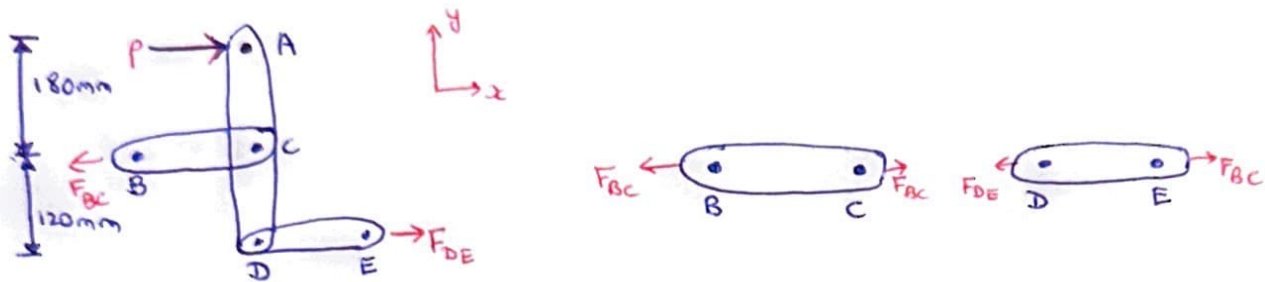


Figure 2: Structure for Problem 2

Solution 2:

FBDs →



Consider the entire structure

- Summing moment about B

$$\sum M_B = 0 = -P_{all}(0.18) + (0.12)F_{DE}$$

$$F_{DE} = 1.5 P_{all} \quad (1)$$

- Summing moment about E

$$\sum M_E = 0 = -P_{all}(0.3) + (0.12)F_{BC}$$

$$F_{BC} = 2.5 P_{all} \quad (2)$$

- For link BC,

$$\sigma_{all} = 500 \text{ MPa} = \frac{F_{BC}}{A} = \frac{2.5 P_{all}}{125 \text{ mm}^2}$$

$$P_{all} = 25 \text{ kN (link BC)} \quad (3)$$

- Pins B and C have shear force F_{BC} acting on them

$$\tau_{all} = 250 \text{ MPa} = \frac{F_{BC}}{A_{pin}} = \frac{2.5 P_{all}}{\frac{\pi}{4} (10)^2 \text{ mm}^2}$$

$$P_{all} \approx 7854 \text{ N (pins B and C)} \quad (4)$$

- For link DE,

$$\sigma_{all} = 500 \text{ MPa} = \frac{F_{DE}}{A} = \frac{1.5 P_{all}}{125 \text{ mm}^2}$$

$$P_{all} \approx 41.67 \text{ kN (link DE)} \quad (5)$$

- Pins D and E have shear force F_{DE} acting on them

$$\tau_{all} = 250 \text{ MPa} = \frac{F_{DE}}{A_{pin}} = \frac{1.5 P_{all}}{\frac{\pi}{4} (10 \text{ mm})^2}$$

$$P_{all} \approx 13090 \text{ N (pins D and E)} \quad (6)$$

★ In order to satisfy all failure criterion, we take the minimum among (3), (4), (5), (6)

$$\therefore P_{all} \approx 7854 \text{ N (at pins B and C)}$$

Problem 3 (10 points):

A biaxial loading, as shown in *figure 3*, acts on a homogeneous plate ABCD. Let $\sigma_z = \sigma_0$. The plate must not have a change in length in the x -direction (or $\epsilon_x = 0$). The plate has a modulus of elasticity E and Poisson's ratio ν . Determine:

- The required magnitude of σ_x in terms of the given parameters,
- The ratio σ_0/ϵ_z .

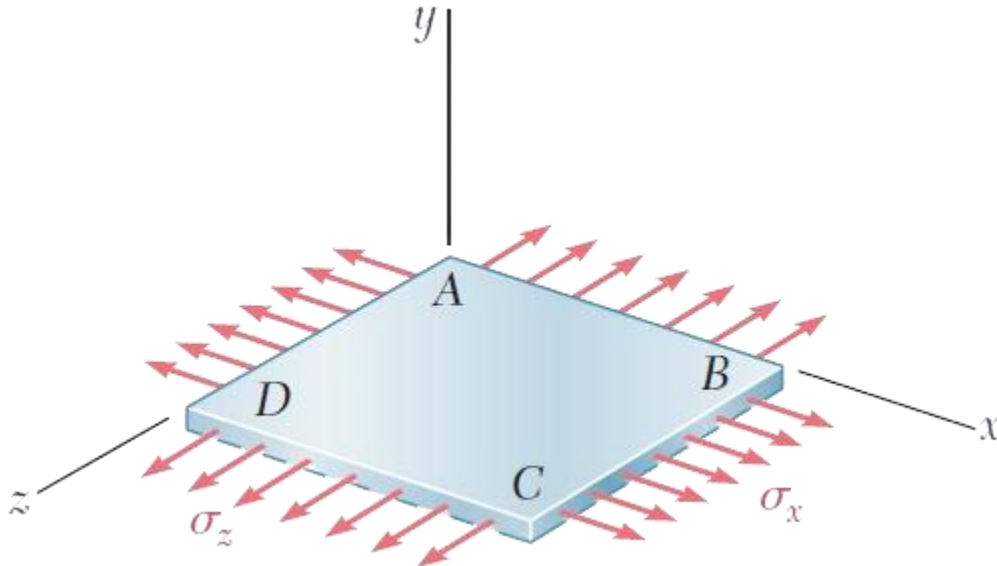
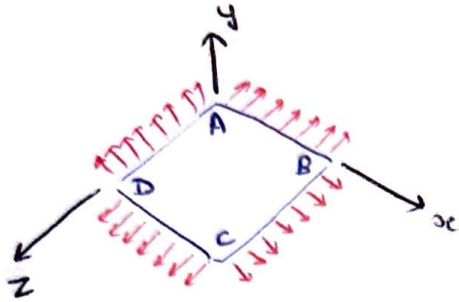


Figure 3: Loading conditions for plate ABCD

Solution 3:



Given,

$$\sigma_z = \sigma_0$$

$$\sigma_y = 0$$

$$\epsilon_x = 0$$

(Biaxial loading)

Now,

$$\epsilon_x = \frac{1}{E} (\sigma_x - \nu (\cancel{\sigma_y} + \sigma_z))$$

$$\epsilon_x = \frac{1}{E} (\sigma_x - \nu \sigma_z)$$

a) $\epsilon_x = 0 \Rightarrow \sigma_x - \nu \sigma_z = 0$

$$\boxed{\sigma_x = \nu \sigma_z = \nu \sigma_0}$$

b) $\epsilon_z = \frac{1}{E} (\sigma_z - \nu (\sigma_x + \cancel{\sigma_y}))$

$$= \frac{1}{E} (\sigma_0 - \nu (\nu \sigma_0))$$

$$= \frac{(1 - \nu^2) \sigma_0}{E}$$

$$\boxed{\frac{\sigma_0}{\epsilon_z} = \frac{E}{1 - \nu^2}}$$

Problem 4 (2.5 points + 2.5 points):

- I. You are given two bars of the same length. One of the bars has a uniform circular cross-section with diameter d and the other has a tapered circular cross-section with end diameters d_1 and d_2 as shown in *figure 4.1*. If they are subjected to the same axial pull, determine the criteria for them to have the same elongation.

- a. $d = \frac{d_1+d_2}{2}$
- b. $d = \sqrt{(d_1 \times d_2)}$
- c. $d = \sqrt{\frac{(d_1 \times d_2)}{2}}$
- d. $d = \sqrt{\frac{(d_1+d_2)}{2}}$

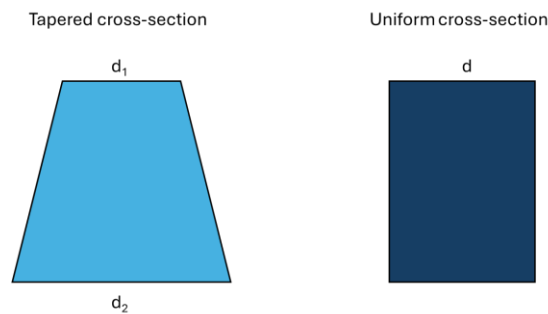


Figure 4.1: Tapered and uniform cross-section

- II. Consider a rigid beam supported in a horizontal position by two rods as shown in *figure 4.2*. The steel rod has a cross-sectional area of 1 cm^2 and Elasticity modulus of 200 GPa , while those of aluminum rod are 2 cm^2 and 100 GPa respectively. For the beam to remain horizontal,
- a. The forces on both sides should be equal.
 - b. The force on aluminum rod should be twice the force on steel rod.
 - c. The force on steel rod should be twice the force on aluminum rod.
 - d. The force P must be at the center of the beam.

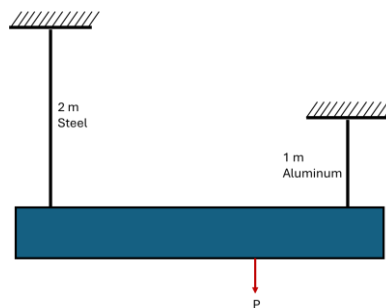


Figure 4.2: Rigid Beam for problem 4.II

Solution 4I

We know that

$$\delta = \frac{FL}{AE}$$

where F = Force or Load

δ = elongation of rod

L = Length of rod

A = Area of cross-section

E = Modulus of Elasticity

For uniform cross-section

$$\delta_1 = \frac{4FL}{\pi d^2 E}$$


For tapered cross-section

Consider an intermediate strip with diameter

$$d(x) = d_1 - kx$$

$$\delta_2 = \int_0^L \frac{4P dx}{\pi E (d_1 - kx)^2}$$

$$= \frac{4P}{\pi E} \left[\frac{-1}{-k(d_1 - kx)} \right] \Big|_0^L = \frac{4P}{\pi E k} \left[\frac{1}{d_1 - kL} - \frac{1}{d_1} \right]$$

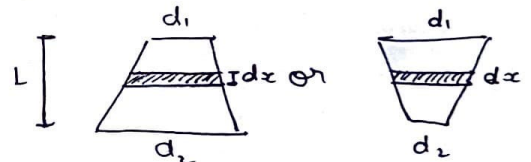
$$\text{But } d_1 - kL = d_2$$

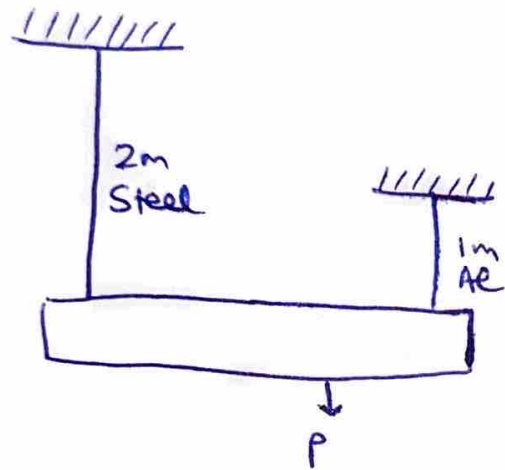
$$\Rightarrow \delta_2 = \frac{4P}{\pi E k} \left(\frac{1}{d_2} - \frac{1}{d_1} \right) = \frac{4P}{\pi E k} \left(\frac{d_1 - d_2}{d_1 k} \right) = \frac{4P k L}{\pi E k d_1 d_2}$$

$$\delta_2 = \frac{4PL}{\pi d_1 d_2 E}$$

$$\delta_1 = \delta_2, \quad P = F, \quad E \text{ is same, } L \text{ is same}$$

$$\Rightarrow \boxed{d = \sqrt{d_1 d_2}} \quad [\text{option B}]$$





For the beam to remain horizontal,

$$\delta_{Ae} = \delta_{Steel}$$

$$\frac{F_{Ae} \times 1}{2 \times 100} = \frac{F_{St} \times 2}{1 \times 200}$$

$$\boxed{F_{Ae} = 2 F_{St}}$$

Option b.)