

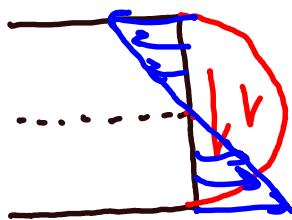
Midterm course evaluations are now open!]

The whole class gets bonus HW points proportional to the number of people who complete the evals:

$$\text{Bonus} = 15 * (\text{proportion of class})$$

For a rectangular cross-section: at the neutral plane, the shear stress is _____ and the normal stress is _____.

- zero, zero
- zero, maximum
- ~~maximum~~, zero ✓
- ~~maximum~~, maximum

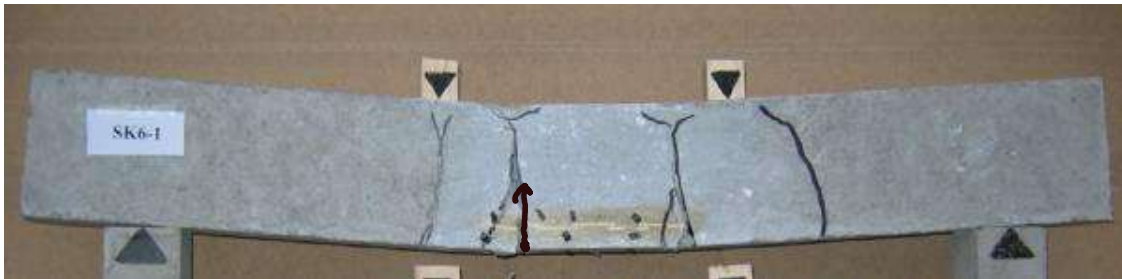


$$\sigma = -\frac{M_y}{I}$$

Failure of Beams



If a material fails due to normal stresses, how will it fail?

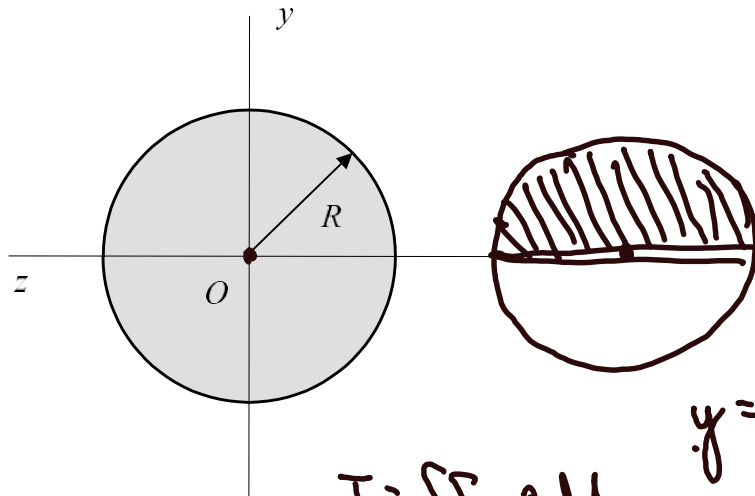


If a material fails due to shear stresses, how will it fail?



Example 10.11

Use the shear stress formula for a general shape cross section developed earlier in the chapter to determine an expression for the maximum shear stress along the symmetry axis y of the circular cross section beam shown below.



$$I = \iint y^2 dA.$$

$$y = r \sin \theta$$

$$\tau(y) = \frac{VA^*\bar{y}^*}{It}$$

$$A^* = \frac{1}{2} \pi R^2$$


$$\bar{y}^* = \int_0^\pi \int_0^R y r dr d\theta$$

$$\bar{y}^* = \frac{4R}{3\pi}$$

$$t = 2R$$

$$I = \frac{\pi}{4} R^4 \quad I_p = \frac{\pi}{2} R^4$$

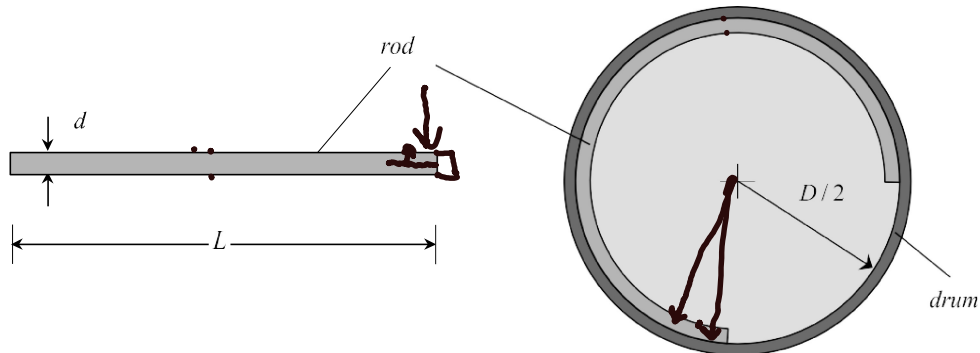
$$\tau_{max} = \frac{V \left(\frac{1}{2} \pi R^2 \right) \left(\frac{4R}{3\pi} \right)}{\left(\frac{\pi}{4} R^4 \right) (2R)} = \frac{4}{3} \frac{V}{\pi R^2} = \boxed{\frac{4}{3} \frac{V}{A}}$$



$$\tau_{max} = \frac{3}{2} \frac{V}{A}$$

Example 10.4

A circular cross-sectioned, straight rod having a diameter of d , a length of L and of a material with a Young's modulus of E is stored by coiling the rod inside of drum with an inside diameter of D . Assuming that the yield strength of rod material is not exceeded, determine the maximum stress in the coiled rod, and the maximum bending moment in the rod.



$$\rho = \frac{D}{2} - \frac{d}{2}$$

$$\epsilon = -\frac{y}{\rho}$$

$$\sigma = -\frac{E y}{\rho}$$

$$\epsilon = -\frac{d}{D-d}$$

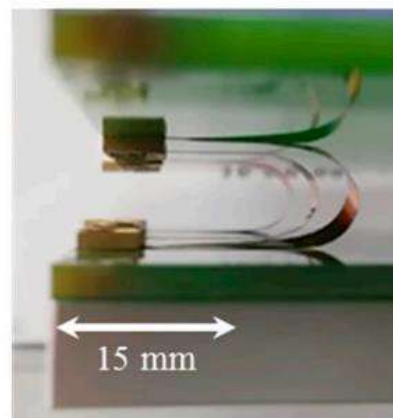
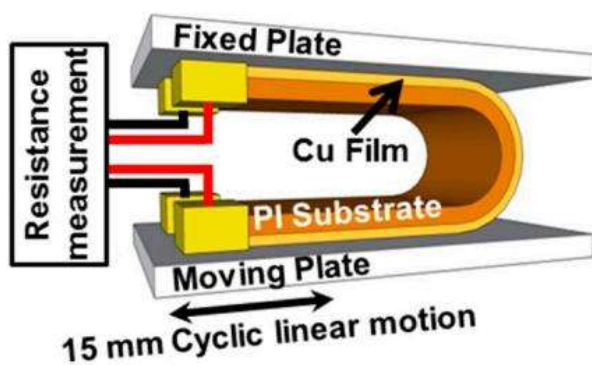
$$\sigma = -\frac{(d/2)E}{\frac{D}{2} - \frac{d}{2}}$$

$$d \ll D$$

$$\Rightarrow \epsilon \sim \frac{d}{D}$$



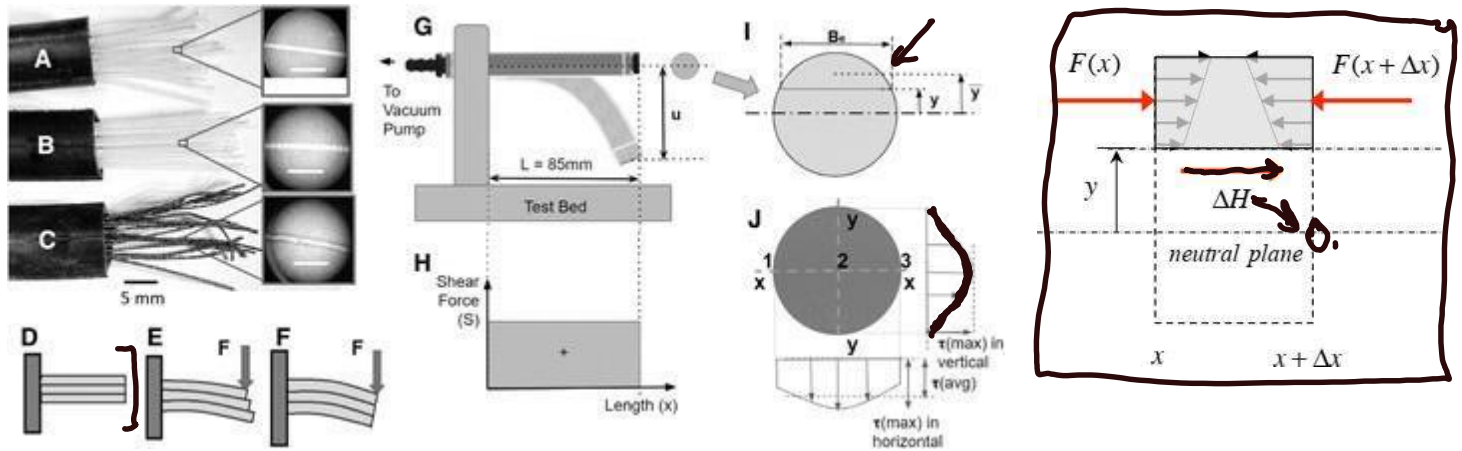
Kim et al, Materials, 12:2490, 2019.



Shear and Normal Stresses in Practical Robots

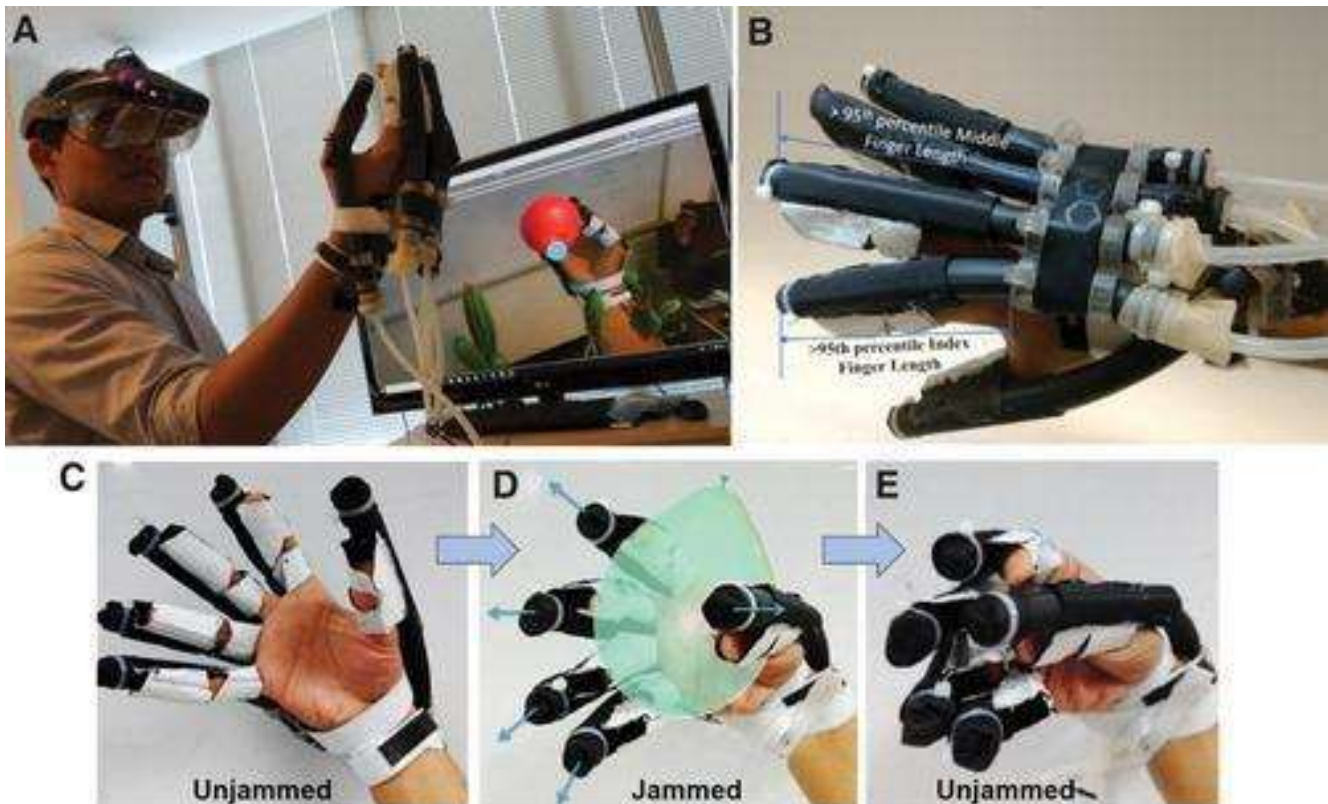
I

D



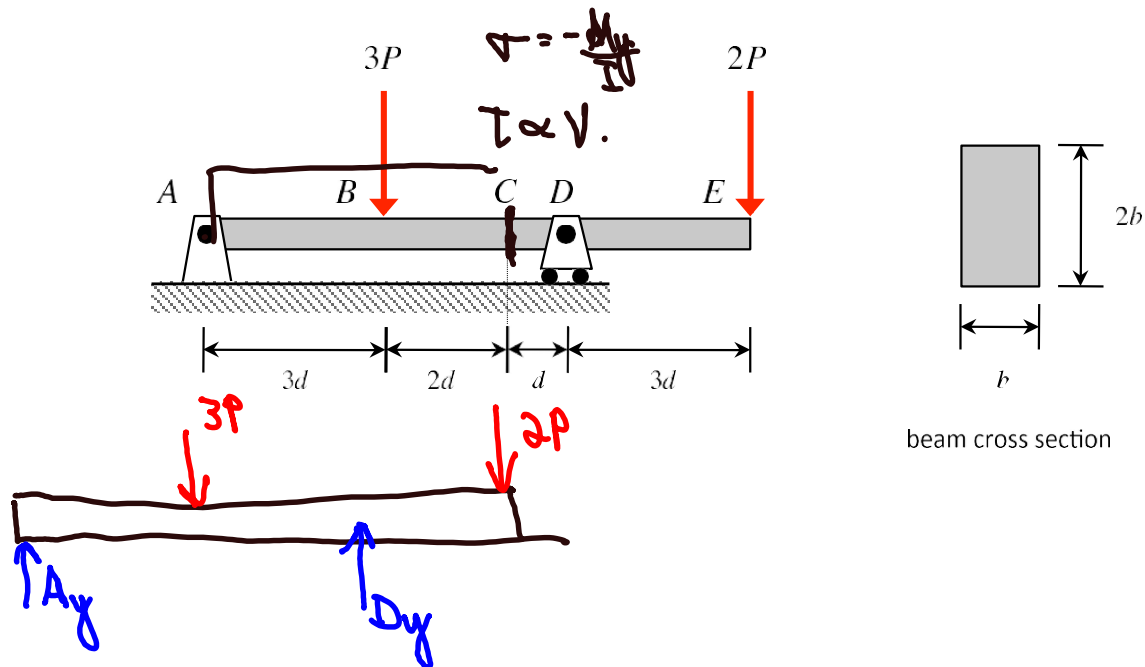
$$\tau_{induced} = k_{correction} \times \frac{SA_e \hat{y}_e}{I_e B_e}, (1) = \frac{VA^* \hat{y}_e}{It.}$$

where A_e is the area of the cross section beyond the section at a distance of y away from the neutral axis, \hat{y}_e is the centroid of that area away from the neutral axis, and B_e is the width of the section at a distance of y from the neutral axis. The accuracy of the above shear stress formula depends on the aspect ratio of the cross section of the ellipse. For very high



Example 10.7

A rectangular cross-section timber beam AE has dimensions and loading shown. Determine the normal and shear stress distributions at location C on the beam.



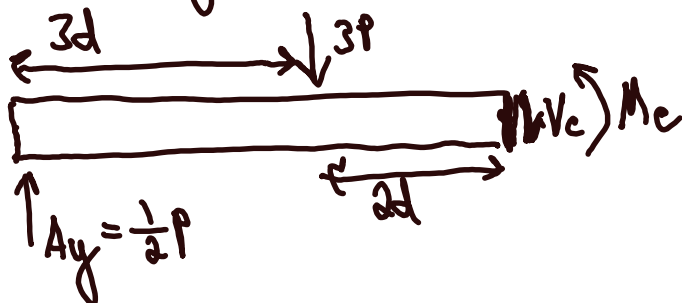
$$(\sum M)_A = -3P(3d) + D_y(6d) - 2P(9d) = 0$$

$$\sum F_y = A_y + D_y - 2P - 3P = 0$$

$$D_y(6d) = 27Pd$$

$$D_y = \frac{9}{2}P$$

$$A_y = 5P - D_y = \frac{1}{2}P$$



$$\sum F_y = A_y - 3P - V_c = 0$$

$$V_c = A_y - 3P = -\frac{5}{2}P$$

$$(\sum M_c) = 3P(2d) - A_y(5d) + M_c = 0$$

$$\frac{12}{2}Pd - \frac{5}{2}Pd + M_c = 0$$

$$M_c = -\frac{7}{2}Pd$$

Normal stresses

$$I = \frac{bh^3}{12} = \frac{b(2b)^3}{12} = \frac{8b^4}{12} = \frac{2b^4}{3}$$

$$\sigma = -\frac{My}{I} = -\left(-\frac{7}{2}Pd\right)y\left(\frac{3}{2b^4}\right) = \frac{21}{4}P\frac{d}{b^4}y$$



Shear stresses

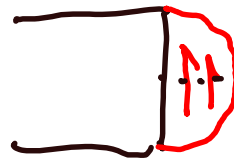
$$\tau = \frac{VA^* \bar{y}^*}{It}$$

$$A^* = b\left(\frac{h}{2} - y\right)$$

$$\bar{y}^* = \frac{1}{2}\left(\frac{h}{2} + y\right)$$

$$t = b$$

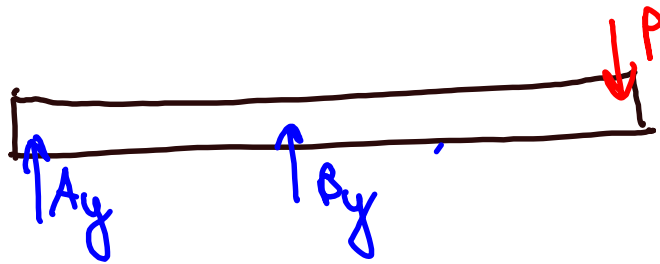
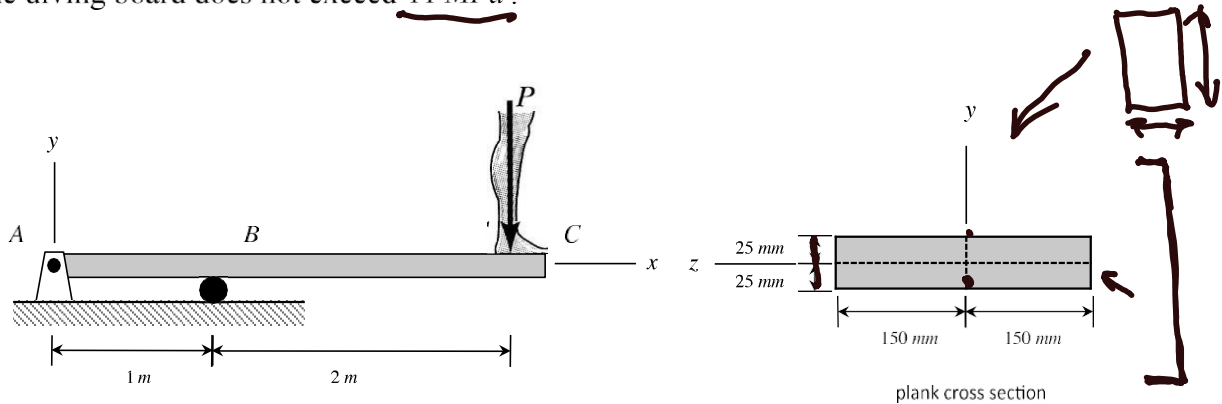
$$\tau = \frac{6}{Ah^2}\left(\frac{h^2}{4} - y^2\right)V$$



$$\underline{\tau_{\max}} = \frac{3}{2}\frac{V}{A} = \frac{3}{2}\left(\frac{3}{2}P\right)\left(\frac{1}{b(2b)}\right) = -\frac{15}{8}\frac{P}{b^2}$$

Example 10.10

A timber plank is to be used as a diving board. The diving board is held down at end A by a steel strap that is secured by anchor bolts and rests on a roller at location B. Calculate the maximum permissible load P_{max} such that the maximum normal stress in the diving board does not exceed 11 MPa.

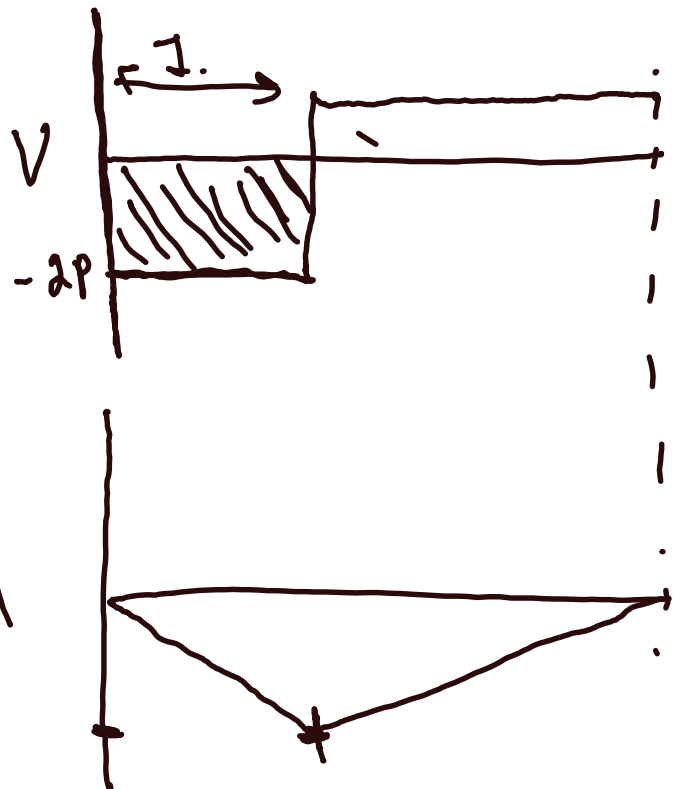


$$(\sum M)_A = B_y(1) - P(3) = 0$$

$$\sum F_y = A_y + B_y - P = 0$$

$$\Rightarrow B_y = 3P \quad A_y = -2P$$

$$M(1) = -2P(1)$$



$$\tau_{\max} = \frac{-M_y}{I} = \frac{-2P(\frac{h}{2})}{(\frac{bh^3}{12})} = -\frac{12P}{bh^2}$$

$$P = \frac{bh^2}{12} |\tau_{\max}| = \frac{(0.3)(0.05)^2}{12} (11 \times 10^6) = 687 \text{ N} = 154 \text{ lbs.}$$

Shear strength of wood $\sim 8 \text{ MPa}$.

$$\tau = \frac{3V}{2A} = \frac{3(-2P)}{2(0.05 \times 0.5)} = 137 \text{ kPa.}$$

\Rightarrow long beams have low shear stress.