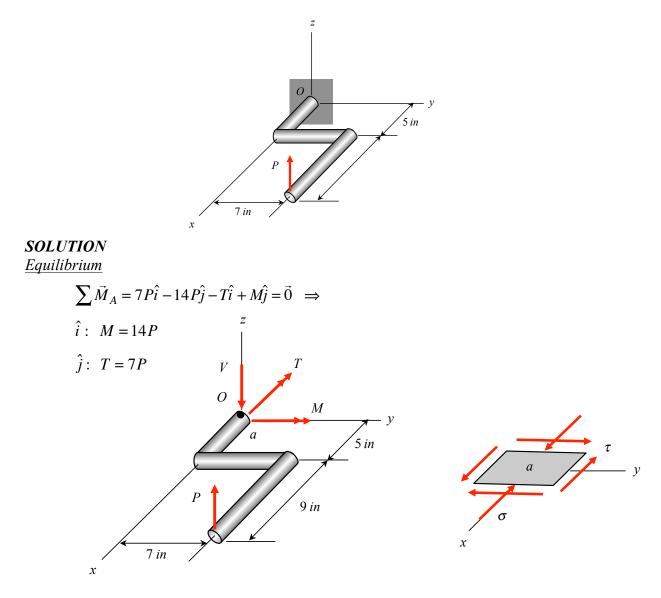
Example 15.4

A crank is fixed to a stationary support at O and is loaded with a force P The crank has a solid cross section of diameter d = 1 in and is made of a ductile material with a yield strength of $\sigma_Y = 100$ ksi. A factor of safety of FS = 2.5 was used in the design of the crank.

Using the maximum shear stress theory, what is the maximum load P allowed?



<u>Stress element</u> (look at stress element on top face of bar at point "a") For this loading (no shear stress from bending at "a" – why?):

$$\sigma = \frac{M(d/2)}{I} = \frac{7Pd}{I}$$

$$\tau = \frac{T(d/2)}{J} = \frac{7Pd}{2J}$$

where:

$$I = \frac{\pi}{64}d^4$$
$$I_P = \frac{\pi}{32}d^4 = 2I$$

Therefore:

$$\tau = \frac{7Pd}{2(\pi d^4 / 32)} = \frac{112P}{\pi d^3}$$
$$\sigma = \frac{7Pd}{\pi d^4 / 64} = \frac{448P}{\pi d^3} = 4\tau$$

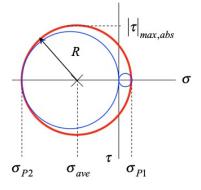
<u>Stress transformation/Mohr's circle</u> From the above state of stress:

$$\sigma_{ave} = -\frac{\sigma}{2} = -224 \frac{P}{\pi d^3}$$

$$R = \sqrt{\left(\frac{\sigma}{2}\right)^2 + \tau^2} = \sqrt{\left(\frac{224P}{\pi d^3}\right)^2 + \left(\frac{112P}{\pi d^3}\right)^2} = 250.4 \frac{P}{\pi d^3}$$

Therefore:

$$\sigma_{P1} = \sigma_{ave} + R = (-224 + 250.4) \frac{P}{\pi d^3} = 26.4 \frac{P}{\pi d^3}$$
$$\sigma_{P2} = \sigma_{ave} - R = (-224 - 250.4) \frac{P}{\pi d^3} = -474.5 \frac{P}{\pi d^3}$$



Since σ_{P1} and σ_{P2} are of opposite signs, then $|\tau|_{\max,abs} = |\tau|_{\max,in-plane} = R$ (see figure):

$$\left|\tau\right|_{max,abs} = R = 250.5 \frac{P}{\pi d^3}$$

Therefore:

$$FS_{S} = \frac{\sigma_{Y}}{2|\tau|_{max,abs}} = \frac{100(10^{3})}{(2)(250.5)} \frac{\pi d^{3}}{P} = 200 \frac{\pi d^{3}}{P} \implies$$
$$P = 200 \frac{\pi d^{3}}{FS_{S}} = 200 \frac{\pi (1)^{3}}{2.5} = 251 \, lb$$

Failure analysis