## Problem 3.1 (10 points)

Rigid bar BD is pinned to ground at end C. The bar is supported by thin rods (1) and (2), where rod (1) has a Young's modulus of E and a cross-sectional area of 2A and rod (2) has a Young's modulus of E and a cross-sectional area of A. Each rod possesses a coefficient of thermal expansion . A load P acts midway between pins C and D on the bar. Assume that the angle of rotation of the bar as a result of the applied load is small and the temperature of both rods is simultaneously increased by $\Delta T$. Ignore the weight of all components of the structure.
(a) Determine the stress in rods (1) and (2).
(b) Determine the angle of rotation of bar BD.


Force - elongation

$$
\begin{aligned}
& e_{1}=\frac{F_{1} L_{1}}{E_{1} A_{1}}+\alpha \Delta T L_{1}=\frac{F_{1} L}{2 E A}+\alpha \Delta T L \quad 1 p+ \\
& e_{2}=\frac{F_{2} L_{2}}{E_{2} A_{2}}+\alpha \Delta T L_{2}=\frac{2 F_{2} L}{E A}+2 \alpha \Delta T L \quad \text { pt }
\end{aligned}
$$

Compatibility
From the structure, $\frac{e_{1}}{2 b}=\frac{e_{2}}{2 b} \Rightarrow e_{1}=e_{2}$ lot

$$
\begin{aligned}
& \frac{F_{1} L}{2 E A}+\alpha \Delta T L=\frac{2 F_{2} L}{E A}+2 \alpha \Delta T L \\
\Rightarrow & F_{1}-4 F_{2}=2 E A \alpha \Delta T \\
\Rightarrow & F_{1}-4 F_{2}=F_{1}-4\left(-\frac{P}{2}-F_{1}\right)=2 E A \alpha \Delta T \\
\Rightarrow & F_{1}=-\frac{2 P}{5}+\frac{2}{5} E A \alpha \Delta T \quad F_{2}=-\frac{P}{10}-\frac{2}{5} E A \alpha \Delta T \\
\Rightarrow & \Delta_{1}=\frac{F_{1}}{A_{1}}=\frac{F_{1}}{2 A}=-\frac{P}{5 A}+\frac{1}{5} E \alpha \Delta T \\
& \Delta_{2}=\frac{F_{2}}{A_{2}}=\frac{F_{2}}{A}=-\frac{P}{10 A}-\frac{2}{5} E \alpha \Delta T
\end{aligned}
$$

b) $\tan \theta=\frac{e_{1}}{2 b}=\frac{e_{2}}{2 b}=\frac{\frac{2 F_{2 L}}{E A}+2 \alpha \Delta T L}{2 b}=\frac{-\frac{P L}{10 E A}-\frac{2}{5} \alpha \Delta T L+\alpha \Delta T L}{b}$

$$
\begin{gathered}
=-\frac{p L}{10 E A b}+\frac{3}{5 b} \alpha \Delta T L \\
\theta=\arctan \left(-\frac{p L}{10 E A b}+\frac{3}{5 b} \alpha \Delta T L\right) \quad 2 p+ \\
\theta \ll 1 \Rightarrow \tan \theta
\end{gathered}
$$

Problem 3.2 (10 points) A rod is made up of elements (1), (2) and (3), as shown below. Element (2) is hollow with outer and inner diameters of 2 d and d, respectively, whereas elements (1) and (3) are solid with diameters of d and 3d, respectively. Elements (1) and (2) are joined by rigid connector D, elements (2) and (3) are joined by rigid connector C, and elements (1) and (3) are connected to ground at ends H and B , respectively. The modulus of elasticity for all three elements is E . The weights of connectors D and C are 2 W and W , respectively, whereas the weights of the rod elements (1), (2) and (3) are to be considered negligible.
(a) Determine the stress in element (3) resulting only from the weights of the connectors (refer to Fig A).
(b) Suppose that an axial load P is applied to connector D in a way that the magnitude of the stress in element (3) is reduced (refer to Fig B). Determine the load value for P such that the magnitude of the compressive stress in (3) reduced by 50 percent from that found in (a).


Fig $A$

FBD

a)

At $D$ :

$$
+\uparrow 工 F_{y}=0: F_{1}-F_{2}-2 w=0 \quad \rightarrow(1)
$$

At $C$ :
3pt: FBD \& equilibrium

$$
\begin{aligned}
& +\uparrow \perp F_{y}=0: F_{2}-W-F_{3}=0 \rightarrow(2) \\
& F_{2}=F_{3}+W \\
& F_{1}=F_{2}+2 W
\end{aligned}
$$

$\Rightarrow$ (2) eqns, (3) variables $\Rightarrow$ it is indeterminate
Compatibility condition

$$
\begin{aligned}
& e_{1}=\frac{F_{1} L_{1}}{A_{1} E_{1}} \quad e_{2}=\frac{F_{2} L_{2}}{A_{2} E_{2}} \quad e_{3}=\frac{F_{3} L_{3}}{A_{3} E_{3}} \\
& C X_{B}^{0}=U_{1} \\
& 0=e_{1}+e_{2}+e_{3}+e_{2}+e_{3} \\
& 0=\frac{F_{1} L_{1}}{A_{1} E}+\frac{F_{2} L_{2}}{A_{2} E}+\frac{F_{3} L_{3}}{A_{3} E} \rightarrow(3) \quad \text { ppt } \\
& \Rightarrow F_{3}=-\frac{57 w}{23} \sim-2.4782 \mathrm{~W} \\
& \Delta_{3}=\frac{F_{3}}{A_{3}}=\frac{-\frac{57 w}{23}}{\left(9 \pi d^{2} / 4\right)} \quad \text { (compression) } \quad 2 p t
\end{aligned}
$$

b)

$$
\begin{aligned}
+\uparrow \Sigma F_{0}=0 \quad & F_{1}-F_{2}-2 w+P=0 \\
& F_{1}=F_{2}+2 w-p=F_{3}+3 w-p
\end{aligned}
$$

compatibility $\Rightarrow e_{1}+e_{2}+e_{3}=0$

$$
\begin{gathered}
\Rightarrow F_{3}=-\frac{57 w}{23}+\frac{18}{23} p \\
\Delta_{3}=\frac{F_{3}}{A_{3}}=\frac{-\frac{57 w}{23}+\frac{18}{23} p}{\frac{9 \pi d^{2}}{4}}=\frac{1}{2}\left(\frac{-\frac{57 w}{23}}{\frac{9 \pi d^{2}}{4}}\right) \\
\Rightarrow \quad \frac{18}{23} p=\frac{57}{46} W \\
\therefore p=\frac{19}{12} W \sim 1.5833 W
\end{gathered}
$$

## Problem 3.3 (10 points)

A composite rod is fixed to the wall at ends A and D , and is made of rods (1), (2), (3) and (4) joined by rigid connectors B and C. Rod (1) of length $L$ has a solid circular cross section, and is made of a material of Young's modulus $2 E$. Rod (2) of length $2 L$ has a solid circular cross section and is composed of a material of Young's modulus $E$. Rod (3) of length $L$ is an outer shell placed concentrically with Rod (4), which is an inner core of length $L$. The outer shell (3) is composed of a material of Young's modulus $E$ and the inner core (4) is composed of a material of Young's modulus $2 E$. Each rod possesses a coefficient of thermal expansion $\alpha$. The cross sections of the 4 rods are shown in figure. In addition, the temperature of Rod $(1)$ is increased by $\Delta T$, while the temperature of other rods is kept constant. Axial loads $3 P$, and $2 P$ are applied to rigid connectors at B and C .
(a) Calculate the axial stresses experienced by rods (1), (2), (3), and (4).
(b) Calculate the displacements of the connectors $u_{B}$, and $u_{C}$.

(3)


$$
\begin{aligned}
& \sum F_{B}=F_{2}-F_{1}+3 P=0 \\
& \Sigma F_{C}=F_{3}+F_{4}-F_{2}-2 P=0 \\
& A_{1}=A_{4}=\frac{1}{4} \pi d^{2} \quad A_{2}=\frac{1}{4} \pi(3 d)^{2}=\frac{9}{4} \pi d^{2} \\
& A_{3}=\frac{1}{4} \pi\left[(2 d)^{2}-d^{2}\right]=\frac{3}{4} \pi d^{2} \\
& e_{1}=\frac{F_{1} L}{2 E A_{1}}+\alpha \Delta T L=\frac{2 F_{1} L}{E \pi d^{2}}+\alpha \Delta T L \quad \text { 0.5pt } \\
& e_{2}=\frac{F_{2}(2 L)}{E A_{2}}=\frac{8 F_{2} L}{9 E \pi d^{2}} \quad 0.5 \mathrm{pt} \\
& e_{3}=\frac{F_{3}(L)}{E A_{3}}=\frac{4 F_{3} L}{3 E \pi d^{2}} \quad 0.5 \mathrm{pt} \\
& e_{4}=\frac{F_{4}(L)}{2 E A_{4}}=\frac{2 F_{4} L}{E \pi d^{2}} \quad 0.5 \mathrm{pt} \\
& u_{0}=u_{A}+e_{1}+e_{2}+e_{3}=0 \quad \because \text { Fixed } A \& D \\
& e_{3}=e_{4} \\
& \Rightarrow e_{1}+e_{2}+e_{3}=\frac{2 F_{1} L}{E \pi d^{2}}+\alpha \Delta T L+\frac{8 F_{2} L}{9 E \pi d^{2}}+\frac{4 F_{3} L}{3 E \pi d^{2}}=0 \\
& \Rightarrow 27 F_{1}+12 F_{2}+18 F_{3}=-\frac{27}{2} \alpha \Delta T E \pi d^{2} \\
& e_{3}=e_{4} \Rightarrow \frac{4 F_{3} L}{3 E \pi d^{2}}=\frac{2 F_{4} L}{E \pi d^{2}} \Rightarrow 2 F_{3}=3 F_{4}
\end{aligned}
$$

$$
\begin{aligned}
\Rightarrow F_{1} & =\frac{78}{83} p-\frac{45}{166} \alpha \Delta T E \pi d^{2} \\
F_{2} & =\frac{-171}{83} p-\frac{45}{166} \alpha \Delta T E \pi d^{2} \\
F_{3} & =\frac{-3}{83} p-\frac{27}{166} \alpha \Delta T E \pi d^{2} \\
F_{4} & =\frac{-2}{83} p-\frac{9}{83} \alpha \Delta T E \pi d^{2} \\
\Delta_{i} & =\frac{F_{i}}{A_{i}} \\
\Rightarrow \sigma_{1} & =\frac{312 p}{83 \pi d^{2}}-\frac{90}{83} \alpha \Delta T E \\
\Delta_{2} & =\frac{-76 p}{83 \pi d^{2}}-\frac{10}{83} \alpha \Delta T E \\
\Delta_{3} & =\frac{-4 p}{83 \pi d^{2}}-\frac{10}{83} \alpha \Delta T E \\
\Delta_{4} & =\frac{-8 p}{83 \pi d^{2}}-\frac{36}{83} \alpha \Delta T E+
\end{aligned}
$$

b)

$$
\begin{aligned}
& u_{B}=e_{1}=\frac{2 F_{1} L}{E \pi d^{2}}+\alpha \Delta T L=\frac{156}{83} \frac{P L}{E \pi d^{2}}+\frac{38}{83} \alpha \Delta T L \quad \text { lpt } \\
& u_{C}=u_{B}+e_{2}=u_{B}+\frac{8 F_{2 L}}{9 E \pi d^{2}}=\frac{4}{83} \frac{P L}{E \pi d^{2}}+\frac{18}{83} \alpha \Delta T L \text { ipt } \\
& u_{D}=u_{C}+e_{3}=0 \quad \text { check! }
\end{aligned}
$$

Problem 3.4 (2.5 + $2.5+2.5$ points)

1. Match the following six structures (a)-(e) with correct option given in i-iii.

i. Statically indeterminate structure
ii. Statically determinate structure
iii. Insufficient information

Number of variables vs number of equation
2. The rod consists of elements (1) and (2) and rigid connectors B and C. Both elements have length L and cross-sectional area A. Element (1) has Young's modulus $E_{1}$, and element (2) has Young's modulus $E_{2}$, with $E_{1}>E_{2}$


Let $F_{1}$ and $F_{2}$ represent the axial forces in members (1) and (2). Choose the correct option.
(a) $F_{1}>F_{2}$
(b) $F_{1}=F_{2}$

Reaction force is the same throughout
(c) $F_{1}<F_{2}$
(d) Insufficient information it's length. Deformation
3. Consider a bar made of two sections fixed at both ends. For section (1) let the length be $L_{1}$, area $A_{1}$, Young's modulus $E_{1}$ and coefficient of thermal expansion $\alpha_{1}$. The corresponding values for section (2) are $L_{2}, A_{2}, E_{2}$ and $\alpha_{2}$. It is known that $L_{1}<L_{2}, E_{1}>E_{2}, A_{1}>A_{2}$ and $\alpha_{1}>\alpha_{2}$. The bar is free of stress at temperature $T_{1}$. Let $\sigma_{1}$ and $\sigma_{2}$ represent the axial stresses in section 1 and 2 , respectively, after the rise in temperature. The temperature is raised from $T_{1}$ to $T_{2}\left(T_{2}>T_{1}\right)$.


If $\delta_{1}$ is the change in length of section 1 and $\delta_{2}$ is the change in length of section 2 , which of the following statements is true?
(a) $\delta_{1}=\delta_{2}=0$
(b) $\delta_{1}+\delta_{2}=0$
(c) $\delta_{1}=\delta_{2} \neq 0$
(d) $\delta_{1}=\frac{E_{1}}{E_{2}} \delta_{2}$

$$
\begin{aligned}
& \delta_{C}=\delta_{A}+\delta_{L}+\delta_{2} \\
& \delta_{C}=\delta_{A}=0 \\
& \text { (Elongation at the support should be zero) }
\end{aligned}
$$

