

Example 16.10

An elastic rod BC of uniform cross section is bent into the form of a three quarter (270°) circle such that its mean radius is R . The rod is fixed to a wall at B and is pinned to a roller at C. The rod is composed of a material of Young's modulus E , and the second area moment of the cross section is I . A downward load P is applied at end C of the rod as shown in Fig 9.3. Assuming that elastic strain energies due to shear and axial loads are negligible as compared to bending strain energy:

- Set up the integral to calculate the total bending strain energy in the rod BC as a function of load P , the unknown reaction F_C at C, and the angle θ .
- Use Castigliano's theorem to determine the reaction force F_C .
- Use Castigliano's theorem to determine the downward deflection of end C.

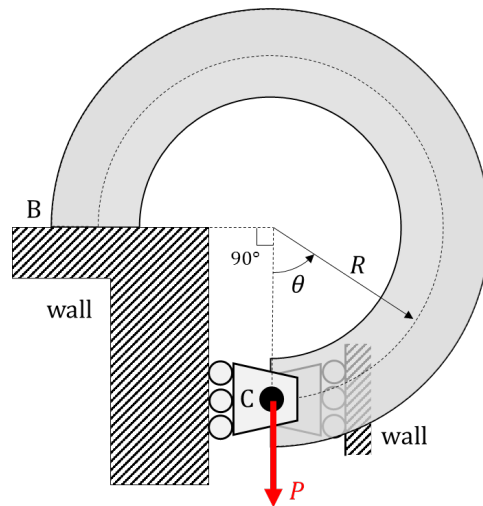


Fig 9.4

Solution

From FBD of segment CD,

$$\begin{aligned} \Sigma M_D &= M_\theta + PR \sin \theta + F_C R(1 - \cos \theta) = 0 \\ \Rightarrow M_\theta &= -PR \sin \theta - F_C R(1 - \cos \theta) \end{aligned}$$

Therefore:

$$U(\theta) = \int_0^{L_{CD}} \frac{M_\theta^2}{2EI} d(L_{CD})$$

where, $d(L_{CD}) = d(R\theta) = R$

$$\Rightarrow U(\theta) = \int_0^\theta \frac{M_\theta^2 R}{2EI} d\theta$$

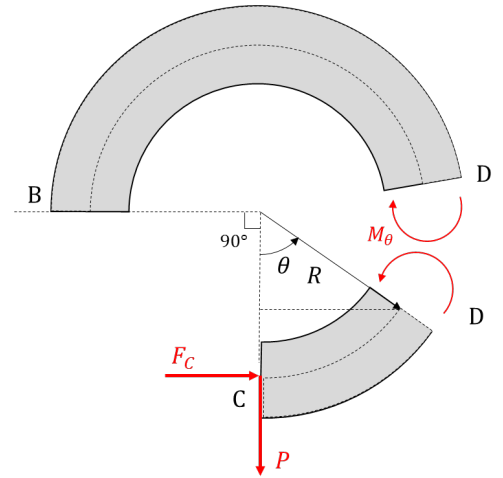
Total strain energy in

BC:

$$U_{BC} = \frac{R}{2EI} \int_0^{\frac{3\pi}{2}} M_\theta^2 d\theta = \frac{R}{2EI} \int_0^{\frac{3\pi}{2}} R^2 [P \sin \theta + F_C(1 - \cos \theta)]^2 d\theta$$

Boundary condition at C: Horizontal deflection at C, $u_C = 0$. Since the horizontal load at C is F_C ,

$$\frac{\partial U_{BC}}{\partial F_C} = 0$$



Using the fundamental theorem of calculation (Leibnitz' rule of differentiation within an integral) on (3.3),

$$\begin{aligned}
 \frac{\partial U_{BC}}{\partial F_C} &= \frac{R}{2EI} \int_0^{\frac{3\pi}{2}} \frac{\partial \{R^2 [P \sin \theta + F_C(1 - \cos \theta)]^2\}}{\partial F_C} d\theta = 0 \\
 &\Rightarrow \frac{R^3}{2EI} \int_0^{\frac{3\pi}{2}} 2(P \sin \theta + F_C(1 - \cos \theta))(R(1 - \cos \theta)) d\theta = 0 \\
 &\Rightarrow \int_0^{\frac{3\pi}{2}} PR \sin \theta (1 - \cos \theta) + F_C R(1 - \cos \theta)^2 d\theta = 0 \\
 &\Rightarrow \int_0^{\frac{3\pi}{2}} PR \sin \theta (1 - \cos \theta) d\theta + \int_0^{\frac{3\pi}{2}} F_C R(1 - \cos \theta)^2 d\theta = 0 \\
 &\Rightarrow \frac{PR}{2} + F_C R \left(2 + \frac{9\pi}{4}\right) = \frac{2P}{4} + F_C \left(\frac{8 + 9\pi}{4}\right) = 0 \\
 &\Rightarrow F_C = -\frac{2P}{8 + 9\pi} = -0.055P \#(4.4)
 \end{aligned}$$

Downward deflection at end C using Castigliano's theorem,

$$\begin{aligned}
 v_C &= \frac{\partial U_{BC}}{\partial P} = \frac{R}{2EI} \int_0^{\frac{3\pi}{2}} \frac{\partial \{R^2 [P \sin \theta + F_C(1 - \cos \theta)]^2\}}{\partial P} d\theta \\
 &\Rightarrow v_C = \frac{R^3}{2EI} \int_0^{\frac{3\pi}{2}} 2(P \sin \theta + F_C(1 - \cos \theta)) \sin \theta d\theta \\
 \Rightarrow v_C &= \frac{PR^3}{EI} \int_0^{\frac{3\pi}{2}} \sin^2 \theta d\theta + \frac{F_C R^3}{EI} \int_0^{\frac{3\pi}{2}} \sin \theta (1 - \cos \theta) d\theta = \frac{PR^3}{EI} \left(\frac{3\pi}{4}\right) + \frac{F_C R^3}{EI} \left(\frac{1}{2}\right) \#(4.5)
 \end{aligned}$$

Substituting (3.4) into (3.5),

$$\Rightarrow v_C = \frac{PR^3}{4EI} (3\pi + 2(-0.055)) = 2.329 \frac{PR^3}{EI}$$