

2/12/2026

# KINEMATICS OF 3D ROTATING FRAMES

Previously, we analyzed systems in which the angular motion  $(\vec{\omega}, \vec{\alpha})$  happened only around the  $\hat{k}$ , which was stationary ( $\dot{\hat{k}} = \hat{k}$ )

For 3D motion, the axis of rotation for  $\vec{\omega}$  will not be stationary

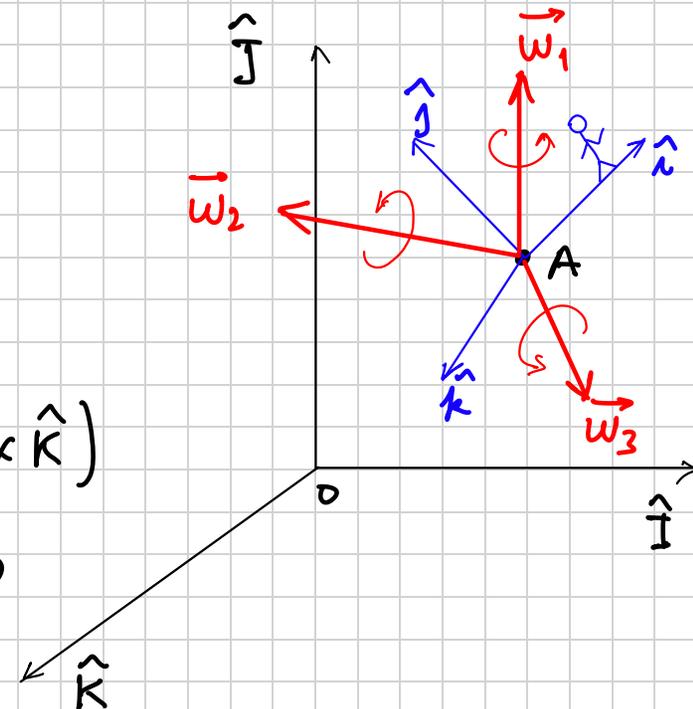
## MOVING REFERENCES IN 2D

$$\vec{\omega} = \dot{\theta} \hat{k}$$

$$\vec{\alpha} = \ddot{\theta} \hat{k} + \dot{\theta} \dot{\hat{k}} = \ddot{\theta} \hat{k} + \dot{\theta} (\vec{\omega} \times \hat{k})$$

$$\text{but } \vec{\omega} \times \hat{k} = \omega \hat{k} \times \hat{k} = 0$$

This is not true for 3D!



For 3D motion, the angular velocity of the observer will be made up of several components

$$\vec{\omega} = \vec{\omega}_1 + \vec{\omega}_2 + \vec{\omega}_3 + \dots$$

Some of these can be about **FIXED** axes and some around **MOVING** axes. It is very important to identify clearly which is which

Example problems here require knowledge of how to write  $\vec{\omega}_s$  and of how to recognize if the rotation is about a fixed or moving axis.

- $x(\hat{i}), y(\hat{j}), z(\hat{k})$  are fixed axes
- $x(\hat{x}), y(\hat{y}), z(\hat{z})$  are moving/rotating axes

# Velocity equation 2D (repeated page)

$$\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$$

But  $\vec{r}_{B/A}$  can be written in terms of the observer's  $xy$  coordinates:

$$\vec{r}_{B/A} = x\hat{i} + y\hat{j}$$

Differentiating  $\vec{r}_B$  with respect to time yields:

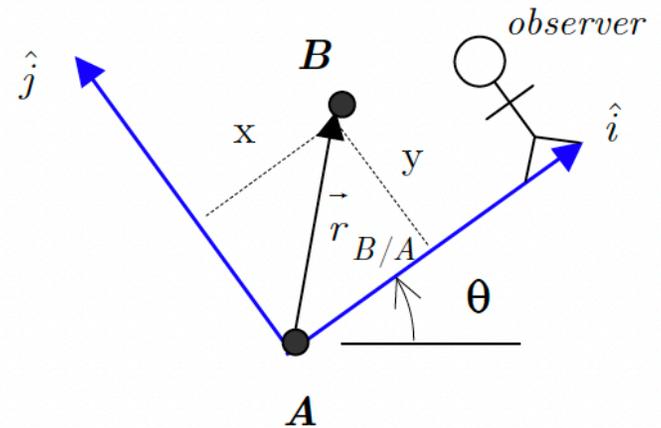
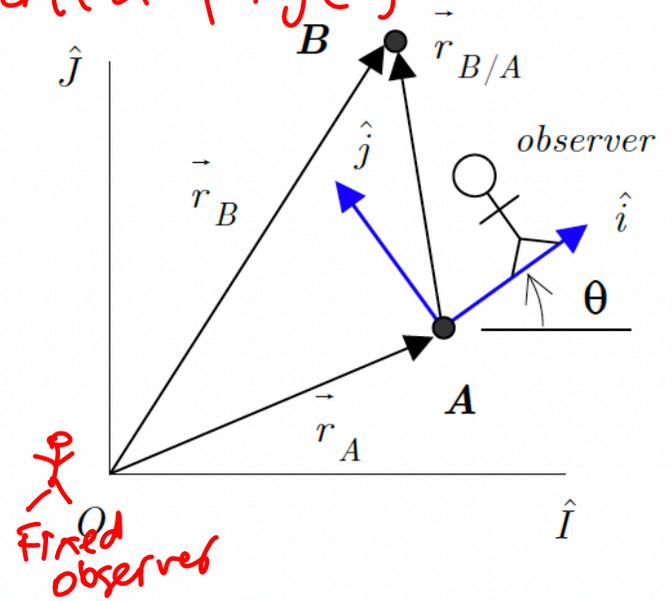
$$\frac{d}{dt} [\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}]$$

$$\vec{v}_B = \vec{v}_A + \dot{x}\hat{i} + x\dot{\hat{i}} + \dot{y}\hat{j} + y\dot{\hat{j}}$$

$$\vec{v}_B = \vec{v}_A + \dot{x}\hat{i} + \dot{y}\hat{j} + x(\vec{\omega} \times \hat{i}) + y(\vec{\omega} \times \hat{j})$$

$$= \vec{v}_A + \dot{x}\hat{i} + \dot{y}\hat{j} + \vec{\omega} \times (x\hat{i} + y\hat{j})$$

$$\vec{v}_B = \vec{v}_A + (\vec{v}_{B/A})_{rel} + \vec{\omega} \times \vec{r}_{B/A}$$



# Velocity equation 3D

$$\vec{v}_B = \vec{v}_A + \vec{v}_{B/A}$$

But  $\vec{v}_{B/A}$  can be written in terms of the observer's xy coordinates:

$$\vec{r}_{B/A} = x\hat{i} + y\hat{j} + z\hat{k}$$

Differentiating  $\vec{r}_B$  with respect to time yields:

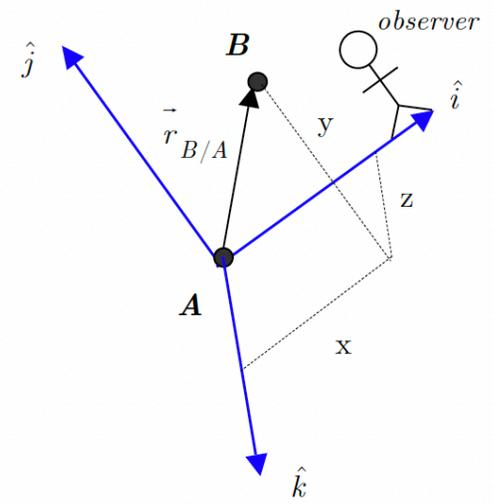
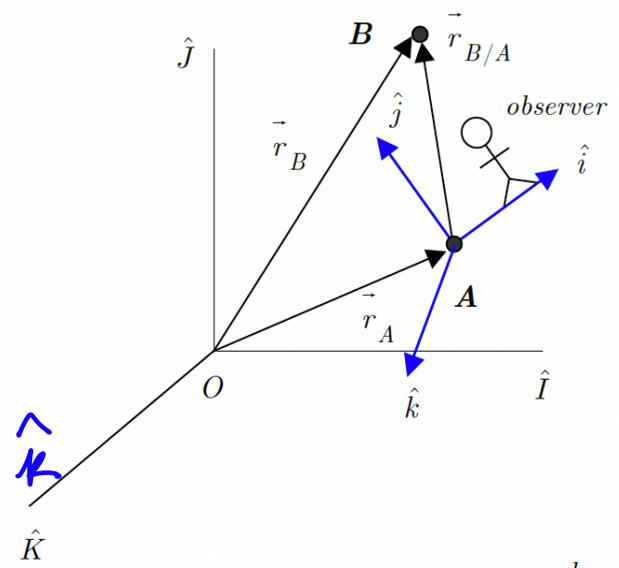
$$\frac{d}{dt} [\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}]$$

$$\vec{v}_B = \vec{v}_A + \dot{x}\hat{i} + x\dot{\hat{i}} + \dot{y}\hat{j} + y\dot{\hat{j}} + \dot{z}\hat{k} + z\dot{\hat{k}}$$

$$\vec{v}_B = \vec{v}_A + \dot{x}\hat{i} + \dot{y}\hat{j} + \dot{z}\hat{k} + x(\vec{\omega} \times \hat{i}) + y(\vec{\omega} \times \hat{j}) + z(\vec{\omega} \times \hat{k})$$

$$= \vec{v}_A + \dot{x}\hat{i} + \dot{y}\hat{j} + \dot{z}\hat{k} + \vec{\omega} \times (x\hat{i} + y\hat{j} + z\hat{k})$$

$$\vec{v}_B = \vec{v}_A + (\vec{v}_{B/A})_{rel} + \vec{\omega} \times \vec{r}_{B/A}$$



Notice that now

$$\left(\vec{v}_{B/A}\right)_{\text{rel}} = \dot{x}\hat{i} + \dot{y}\hat{j} + \dot{z}\hat{k}$$

is the relative velocity seen by the observer

### Acceleration equation 3D

$$\frac{d}{dt} \left[ \vec{v}_B = \vec{v}_A + \left(\vec{v}_{B/A}\right)_{\text{rel}} + \vec{\omega} \times \vec{r}_{B/A} \right]$$

$$\vec{a}_B = \vec{a}_A + \frac{d}{dt} \left(\vec{v}_{B/A}\right)_{\text{rel}} + \frac{d}{dt} \left(\vec{\omega} \times \vec{r}_{B/A}\right)$$

$$\vec{a}_B = \vec{a}_A + \frac{d}{dt} (\dot{x}\hat{i} + \dot{y}\hat{j} + \dot{z}\hat{k}) + \frac{d\vec{\omega}}{dt} \times \vec{r}_{B/A} + \vec{\omega} \times \frac{d}{dt} (\vec{r}_{B/A})$$

PRODUCT RULE

from the velocity derivation:

$$\frac{d}{dt} \left[ \vec{r}_{B/A} \right] = \left(\vec{v}_{B/A}\right)_{\text{REL}} + \vec{\omega} \times \vec{r}_{B/A}$$

$$\vec{a}_B = \vec{a}_A + \underbrace{(\ddot{x}\hat{i} + \ddot{y}\hat{j} + \ddot{z}\hat{k})}_{\text{red}} + \underbrace{(\dot{x}\hat{i} + \dot{y}\hat{j} + \dot{z}\hat{k})}_{\text{blue}} + \vec{\alpha} \times \vec{r}_{B/A} + \vec{\omega} \times \left[ (\vec{N}_{B/A})_{\text{REL}} + \vec{\omega} \times \vec{r}_{B/A} \right]$$

$$\vec{a}_B = \vec{a}_A + \underbrace{(\vec{a}_{B/A})_{\text{REL}}}_{\text{red}} + \underbrace{\dot{x}(\vec{\omega} \times \hat{i}) + \dot{y}(\vec{\omega} \times \hat{j}) + \dot{z}(\vec{\omega} \times \hat{k})}_{\text{blue}} + \vec{\alpha} \times \vec{r}_{B/A} + \vec{\omega} \times \left[ (\vec{N}_{B/A})_{\text{REL}} + \vec{\omega} \times \vec{r}_{B/A} \right]$$

$$\vec{a}_B = \vec{a}_A + (\vec{a}_{B/A})_{\text{REL}} + \underbrace{\vec{\omega} \times (\dot{x}\hat{i} + \dot{y}\hat{j} + \dot{z}\hat{k})}_{\text{blue}} + \vec{\alpha} \times \vec{r}_{B/A} + \vec{\omega} \times \left[ (\vec{N}_{B/A})_{\text{REL}} + \vec{\omega} \times \vec{r}_{B/A} \right]$$

$$\vec{a}_B = \vec{a}_A + (\vec{a}_{B/A})_{\text{REL}} + \vec{\omega} \times (\vec{N}_{B/A})_{\text{REL}} + \vec{\alpha} \times \vec{r}_{B/A} + \vec{\omega} \times (\vec{N}_{B/A})_{\text{REL}} + \vec{\omega} \times [\vec{\omega} \times \vec{r}_{B/A}]$$

$$\vec{a}_B = \vec{a}_A + (\vec{a}_{B/A})_{\text{REL}} + \vec{\alpha} \times \vec{r}_{B/A} + 2\vec{\omega} \times (\vec{N}_{B/A})_{\text{REL}} + \vec{\omega} \times [\vec{\omega} \times \vec{r}_{B/A}]$$

→ Relative acceleration of B  
as seen by the observer.

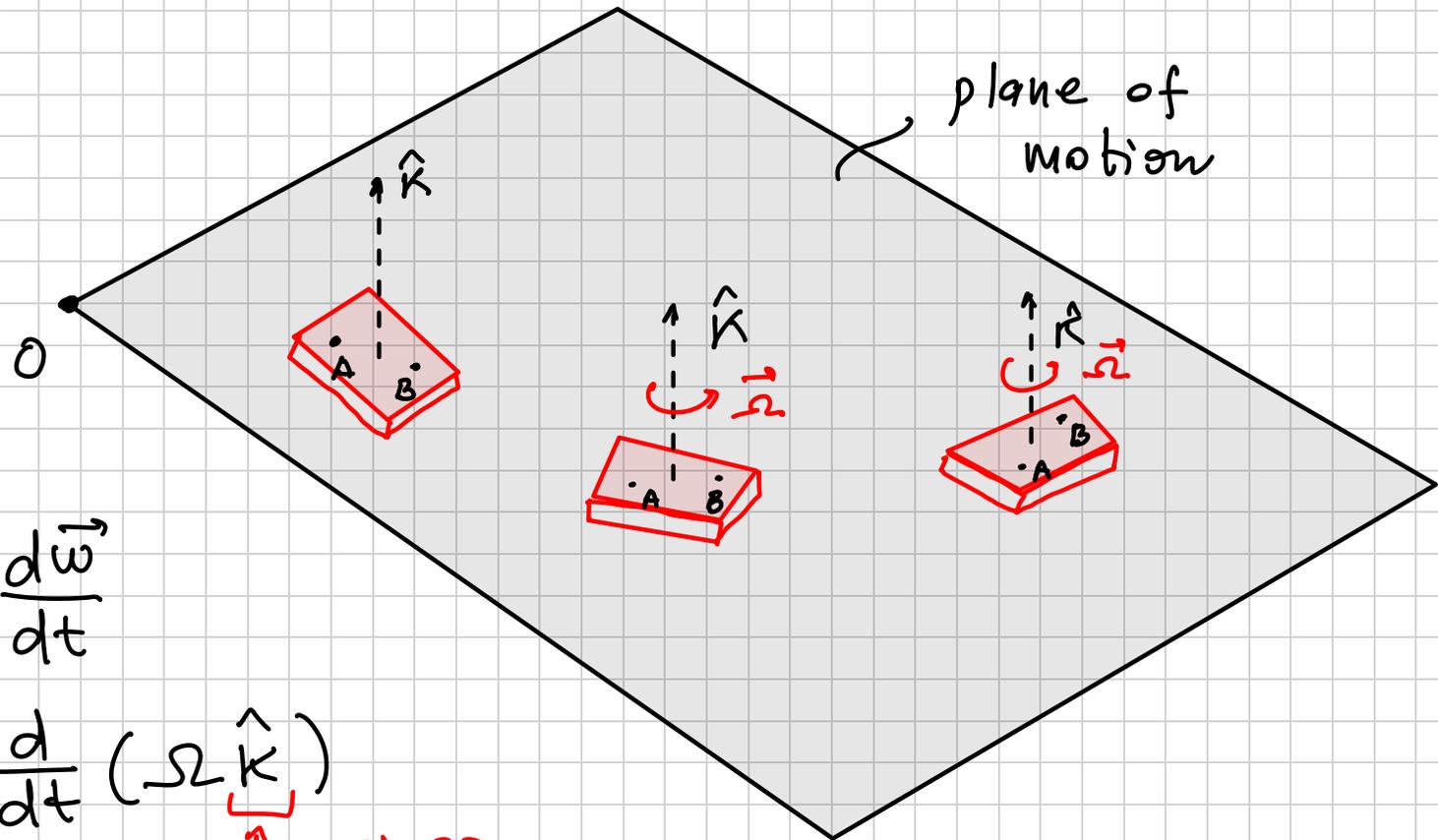
In 3D motion,  $\vec{\omega} \times (\vec{\omega} \times \vec{r}_{B/A}) \neq -\omega^2 \vec{r}_{B/A}$

In 3D motion,  $\vec{\omega} \neq \dot{\theta} \hat{k}$

# Angular acceleration of rotating frame

$$\vec{\alpha} = \frac{d}{dt} \vec{\omega}$$

For 2D problems, the moving reference frame is rotating @ a FIXED axis ( $\perp$  to the plane of motion).



$$\alpha = \frac{d\vec{\omega}}{dt}$$

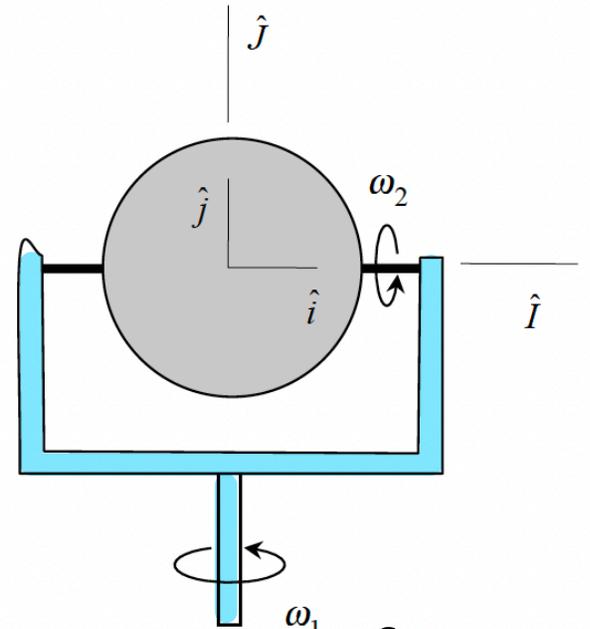
$$= \frac{d}{dt} (\Omega \hat{k})$$

$$= \dot{\Omega} \hat{k}$$

↑ FIXED

For 3D Problems  $\frac{d\vec{\omega}}{dt}$  is not straight forward

Consider the gimbal below: the blue frame rotates about the fixed  $\hat{j}$  axis, and the disk rotates about the moving  $\hat{i}$  axis.



$$\Rightarrow \vec{\omega}_{\text{TOTAL}} = \omega_1 \hat{j} + \vec{\omega}_2 \hat{i}$$

$$\vec{\alpha} = \frac{d}{dt} (\vec{\omega}_{\text{TOT}}) = \dot{\omega}_1 \hat{j} + \omega_1 \dot{\hat{j}} + \dot{\omega}_2 \hat{i} + \omega_2 \dot{\hat{i}}$$

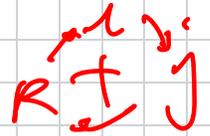
$\underbrace{\omega_2 \dot{\hat{i}}}_{\vec{\omega}_{\text{TOT}} \times \hat{i}}$

$$\vec{\alpha} = \dot{\omega}_1 \hat{j} + \dot{\omega}_2 \hat{i} + \omega_2 (\vec{\omega}_{\text{TOT}} \times \hat{i})$$

$$\vec{\alpha} = \dot{\omega}_1 \hat{j} + \dot{\omega}_2 \hat{i} + \omega_2 [(\omega_1 \hat{j} + \omega_2 \hat{i}) \times \hat{i}]$$

$$\vec{\alpha} = \dot{\omega}_1 \hat{j} + \dot{\omega}_2 \hat{i} - \omega_2 \omega_1 (\hat{j} \times \hat{i}) \quad (\hat{j} = \hat{j})$$

$$\Rightarrow \vec{\alpha} = \dot{\omega}_1 \hat{j} + \dot{\omega}_2 \hat{i} - \omega_2 \omega_1 \hat{k}$$



So, even if one has constant rates of change of the angular velocities,  $\alpha$  may not be zero!

$$\vec{\alpha} = -\omega_2 \omega_1 \hat{k}$$

Summary:

$$\vec{v}_B = \vec{v}_A + (\vec{v}_{B/A})_{rel} + \vec{\omega} \times \vec{r}_{B/A}$$

$$\vec{a}_B = \vec{a}_A + (\vec{a}_{B/A})_{rel} + \vec{\alpha} \times \vec{r}_{B/A} + 2\vec{\omega} \times \vec{v}_{B/A} + \vec{\omega} \times [\vec{\omega} \times \vec{r}_{B/A}]$$

and  $\vec{\alpha}$  may not be zero even if  $\dot{\omega}_1 = \dot{\omega}_2 = 0$

and  $\omega_{TOT} = \omega_1 + \omega_2 + \dots$

An excavator is rotating its turret at a constant  $\Omega \hat{K}$  and lifting its boom at a constant  $\dot{\theta} \hat{i}$ . The magnitude of the total angular acceleration that the load is “feeling” is:

- A) Since both angular velocities are constant, obviously the total  $|\vec{\alpha}|$  should be zero.
- B) Would be the sum of both rates of change of the angular velocities.
- C) Proportional to the product of  $\dot{\theta}$ , and  $\Omega$ .
- D) More information is needed to determine the resulting angular acceleration magnitude.

$$\omega = \Omega \hat{K} + \dot{\theta} \hat{i}$$

$$\alpha = ?$$

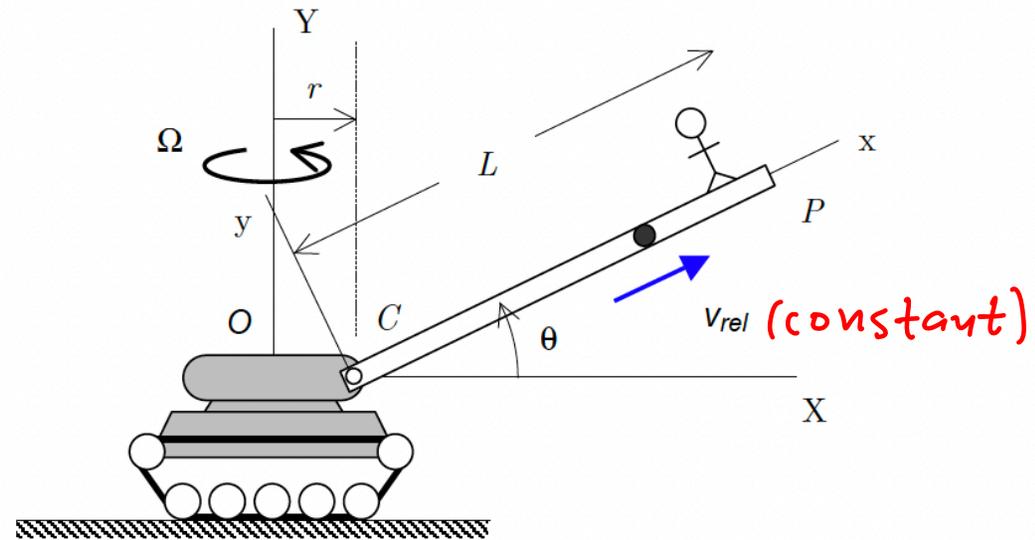
### Example 3.B.4

**Given:** The turret on a tank is rotating about a fixed vertical axis at a constant rate of  $\Omega = 0.4$  rad/s. The barrel is being raised at a constant rate of  $\dot{\theta} = 0.4$  rad/s. A cannon shell is fired with a constant muzzle speed of  $v_{rel} = 200$  ft/s relative to the barrel. The observer and the  $xyz$  axes are attached to the barrel, while the  $XYZ$  axes are fixed. Here,  $r = 3$  ft and  $L = 15$  ft.

The tank is not moving at the instant shown

**Find:**

- The angular velocity of the barrel at the instant shown;
- The angular acceleration of the barrel at the instant shown; and
- The acceleration of the shell as it leaves the barrel at P.



Solution:

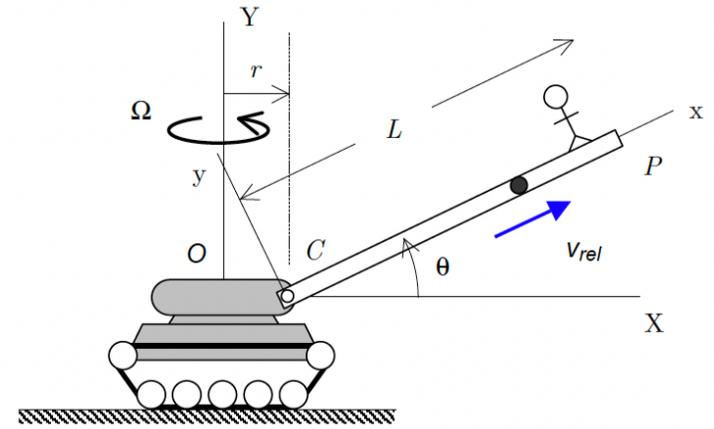
$$\vec{\omega}_{TOT} = \Omega \hat{j} + \dot{\theta} \hat{k}$$

$$\vec{\alpha} = \frac{d}{dt}(\omega_{TOT}) = \cancel{\dot{\Omega}} \hat{j} + \Omega \hat{j} + \cancel{\ddot{\theta}} \hat{k} + \dot{\theta} \hat{k} \neq 0$$

REMEMBER  $\dot{\hat{k}} = \vec{\omega}_{TOT} \times \hat{k}$

$$\begin{aligned}\vec{\alpha} &= \dot{\theta} (\vec{\omega}_{TOT} \times \hat{k}) \\ &= \dot{\theta} [(\Omega \hat{j} + \dot{\theta} \hat{k}) \times \hat{k}] \\ \hat{K} &= \hat{k}\end{aligned}$$

$$\vec{\alpha} = \dot{\theta} \Omega \hat{i}$$



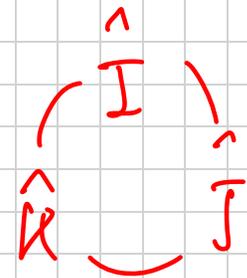
Only now we can approach the accel. eqn.

$$\vec{a}_P = \vec{a}_C + \cancel{(\vec{a}_{P/C})_{rel}} + \vec{\alpha} \times \vec{r}_{P/C} + 2\vec{\omega}_{TOT} \times (\vec{v}_{P/C})_{rel} + \vec{\omega}_T \times [\vec{\omega}_T \times \vec{r}_{P/C}]$$

$$\vec{a}_C = \cancel{\vec{a}_O} + \cancel{\alpha_O} \times \vec{r}_{C/O} + \vec{\omega}_{CO} \times (\vec{\omega}_{CO} \times \vec{r}_{C/O})$$

$$\vec{a}_C = \Omega \hat{j} \times (\Omega \hat{j} \times r \hat{i})$$

$$\vec{a}_C = -\Omega r \hat{k}$$

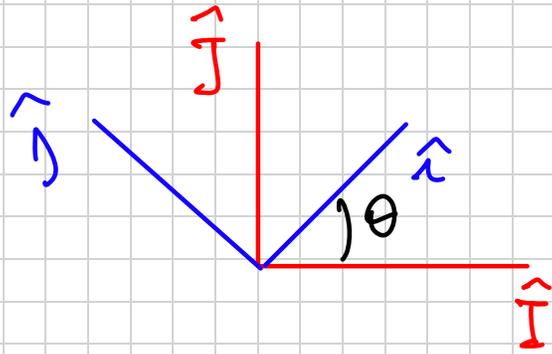


$$(\vec{a}_{P/C})_{rel} = \vec{0} \quad (\text{constant muzzle velocity})$$

$$\vec{r}_{P/C} = L \hat{i}$$

$$(\vec{v}_p/c)_{\text{rel}} = v_{\text{REL}} \hat{\lambda}$$

$$\Rightarrow \vec{a}_p = -\Omega^2 r \hat{I} + \dot{\theta} \Omega \hat{I} \times L \hat{\lambda} + 2(\Omega \hat{J} + \dot{\theta} \hat{K}) \times v_{\text{REL}} \hat{\lambda} + (\Omega \hat{J} + \dot{\theta} \hat{K}) \times [(\Omega \hat{J} + \dot{\theta} \hat{K}) \times L \hat{\lambda}]$$



$$\hat{\lambda} = \cos \theta \hat{I} + \sin \theta \hat{J}$$

$$\Rightarrow \vec{a}_p = -\Omega^2 r \hat{I} + \dot{\theta} \Omega \hat{I} \times (L \cos \theta \hat{I} + L \sin \theta \hat{J}) + 2(\Omega \hat{J} + \dot{\theta} \hat{K}) \times v_{\text{REL}} (\cos \theta \hat{I} + \sin \theta \hat{J}) + (\Omega \hat{J} + \dot{\theta} \hat{K}) \times [(\Omega \hat{J} + \dot{\theta} \hat{K}) \times (L \cos \theta \hat{I} + L \sin \theta \hat{J})]$$

$$\Rightarrow \vec{a}_p = -\Omega^2 r \hat{I} + \dot{\theta} \Omega L \sin \theta \hat{K} +$$

$$- 2 \Omega N_{REL} \cos \theta \hat{K} + 2 \dot{\theta} N_{REL} \cos \theta \hat{J} - 2 \dot{\theta} N_{REL} \sin \theta \hat{I}$$

$$+ (\Omega \hat{J} + \dot{\theta} \hat{K}) \times [-\Omega L \cos \theta \hat{K} + \dot{\theta} L \cos \theta \hat{J} - \dot{\theta} L \sin \theta \hat{I}]$$

$$\Rightarrow \vec{a}_p = -\Omega^2 r \hat{I} + \dot{\theta} \Omega L \sin \theta \hat{K} + 2 \Omega N_{REL} \cos \theta \hat{K}$$

$$+ 2 \dot{\theta} N_{REL} \cos \theta \hat{J} - 2 \dot{\theta} N_{REL} \sin \theta \hat{I}$$

$$- \Omega^2 L \cos \theta \hat{I} - \Omega \dot{\theta} L \sin \theta \hat{K} - \dot{\theta}^2 L \cos \theta \hat{I} - \dot{\theta}^2 L \sin \theta \hat{J}$$