

# *ME 274: Basic Mechanics II*

Lecture 12: Moving Reference Frame Kinematics



School of Mechanical Engineering

# *Announcements*

## **Exam 1 info:**

- Exam 1, Thurs. 2/12, 8 – 9:30, MA 175
- Students with exam accommodations: HIKS G980D, 6:30PM – reminder to email Dr. Krousgrill
- Exam review session Tuesday 2/10, 7pm over Zoom (link on course website on “Exams” page)

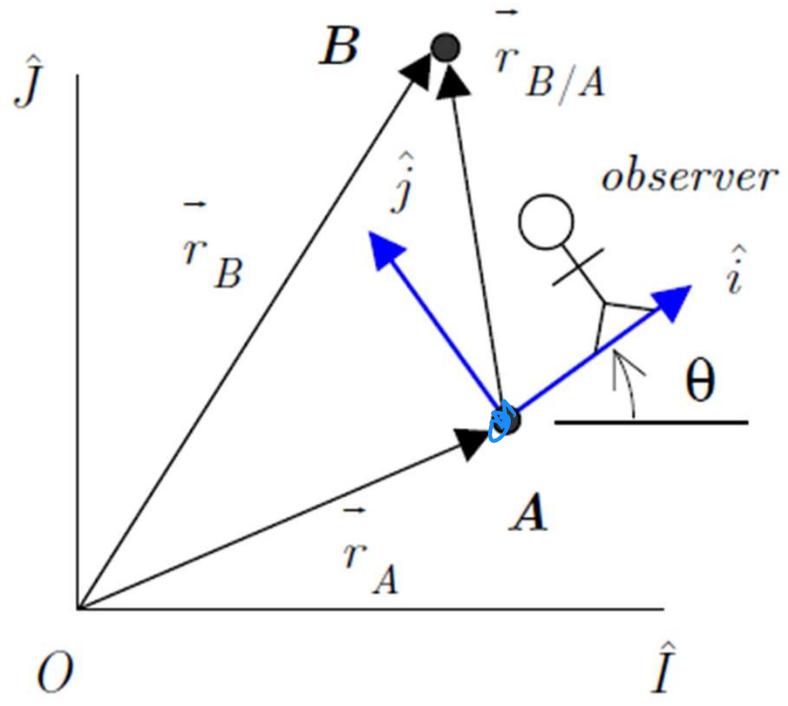
## **Homework and class updates:**

- No class Friday, 2/13 to account for evening exam
- HW released today (2.C, 2.D) **due Friday 2/13**
- HW released on Wednesday (2.E, 2.F) **due Monday 2/16**
- **Reminder to use correct HW formatting!**
- Office hrs: T 9-10:30, W 3:30-4:20, Th 3-4:30

# Moving Reference Frames - Overview

- Stationary axis  $\rightarrow XYZ$  axis  $\rightarrow$  point  $B$  as seen by an outside observer
- Moving reference frame  $\rightarrow xyz$  axis  $\rightarrow$  point  $B$  as seen from an observer at point  $A$
- The angular speed of the observer is given by the time rate of change of the angle  $\theta$  between the fixed and moving reference frame  $\rightarrow \vec{\omega} = \dot{\theta} \hat{k}$

$\vec{\alpha} = \ddot{\theta} \hat{k}$  



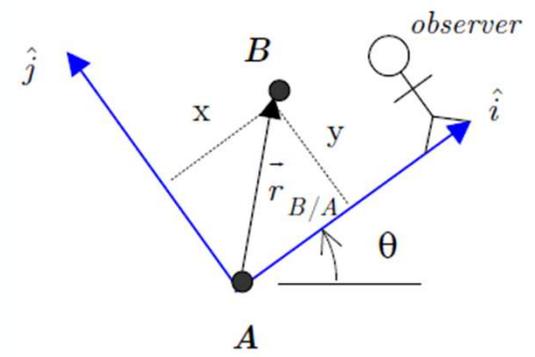
Relating velocity and acceleration of pts.  $B$  and  $A$  :

$$\vec{v}_B = \vec{v}_A + (\vec{v}_{B/A})_{rel} + \vec{\omega} \times \vec{r}_{B/A}$$

$$\vec{a}_B = \vec{a}_A + (\vec{a}_{B/A})_{rel} + \vec{\alpha} \times \vec{r}_{B/A} + \underbrace{2\vec{\omega} \times (\vec{v}_{B/A})_{rel}}_{\text{Coriolis acceleration}} + \vec{\omega} \times [\vec{\omega} \times \vec{r}_{B/A}]$$

Where  $(\vec{v}_{B/A})_{rel}, (\vec{a}_{B/A})_{rel}$  are the velocity and acceleration of point  $B$  as observed from  $A$ .

Remember pt  $A$  must be on the same reference frame as the observer!



$$(\vec{v}_{B/A})_{rel} = x \hat{i} + y \hat{j}$$

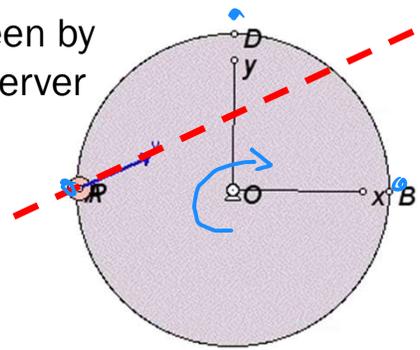
$$(\vec{a}_{B/A})_{rel} = \ddot{x} \hat{i} + \ddot{y} \hat{j}$$

# The Coriolis Component of Acceleration

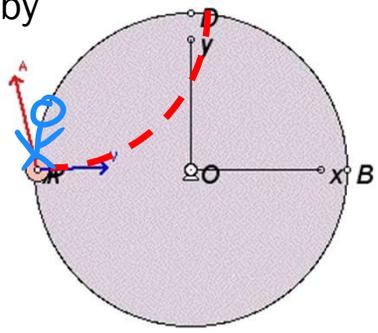
- The Coriolis component arises when a point has a nonzero velocity relative to a rotating reference frame.
- Although the point may be moving in a straight line with constant velocity in an inertial frame, the rotating observer sees the direction of that relative velocity continuously change as the reference axes rotate.

Ex 1: Merry-go-round

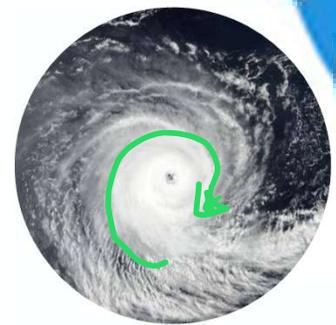
Motion of  $P$  seen by stationary observer



Motion of  $P$  seen by moving observer



Ex 2: Weather Systems



### Question C3.3

Sprinkler arm OA is pinned to a cart at point O. The cart moves to the right with a speed of  $v_{cart}$  with  $\dot{v}_{cart} = 2 \text{ ft/s}^2 = \text{constant}$ . Fluid flows through the sprinkler arm at a rate of  $\dot{d}$  with  $\ddot{d} = -3 \text{ ft/s}^2 = \text{constant}$ . The sprinkler arm is being raised at a constant rate of  $\dot{\theta} = 4 \text{ rad/s}$ . An observer and  $xyz$  coordinate system are attached to the sprinkler arm, as shown in the figure below. The following equation is to be used to find the acceleration of a pellet P that flows with the fluid in the arm:

$$\vec{a}_P = \vec{a}_O + (\vec{a}_{P/O})_{rel} + \vec{\alpha} \times \vec{r}_{P/O} + 2\vec{\omega} \times (\vec{v}_{P/O})_{rel} + \vec{\omega} \times [\vec{\omega} \times \vec{r}_{P/O}]$$

Provide numerical values for the following terms when:  $d = 3 \text{ ft}$ ,  $v_{cart} = 3 \text{ ft/s}$ ,  $\dot{d} = 5 \text{ ft/s}$  and  $\theta = 90^\circ$ .

$$\vec{a}_O = 2 \hat{i} \rightarrow 2 \hat{j}$$

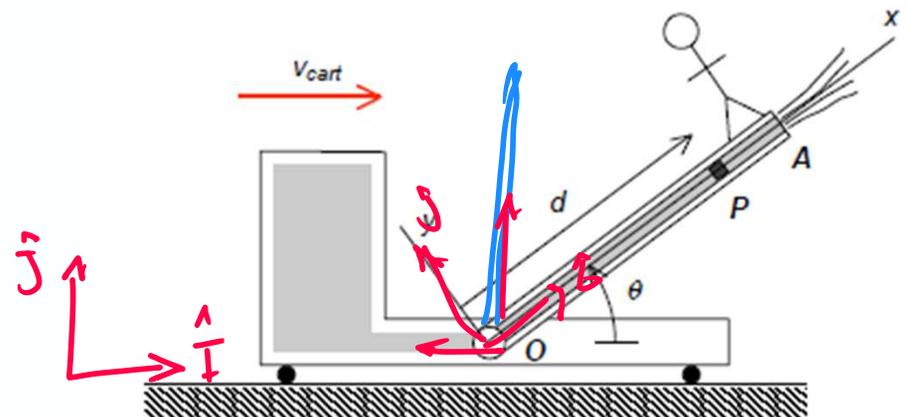
$$\vec{\omega} = 4 \hat{k}$$

$$\vec{\alpha} = \vec{0}$$

$$(\vec{v}_{P/O})_{rel} = \dot{d} \hat{i} = 5 \hat{i}$$

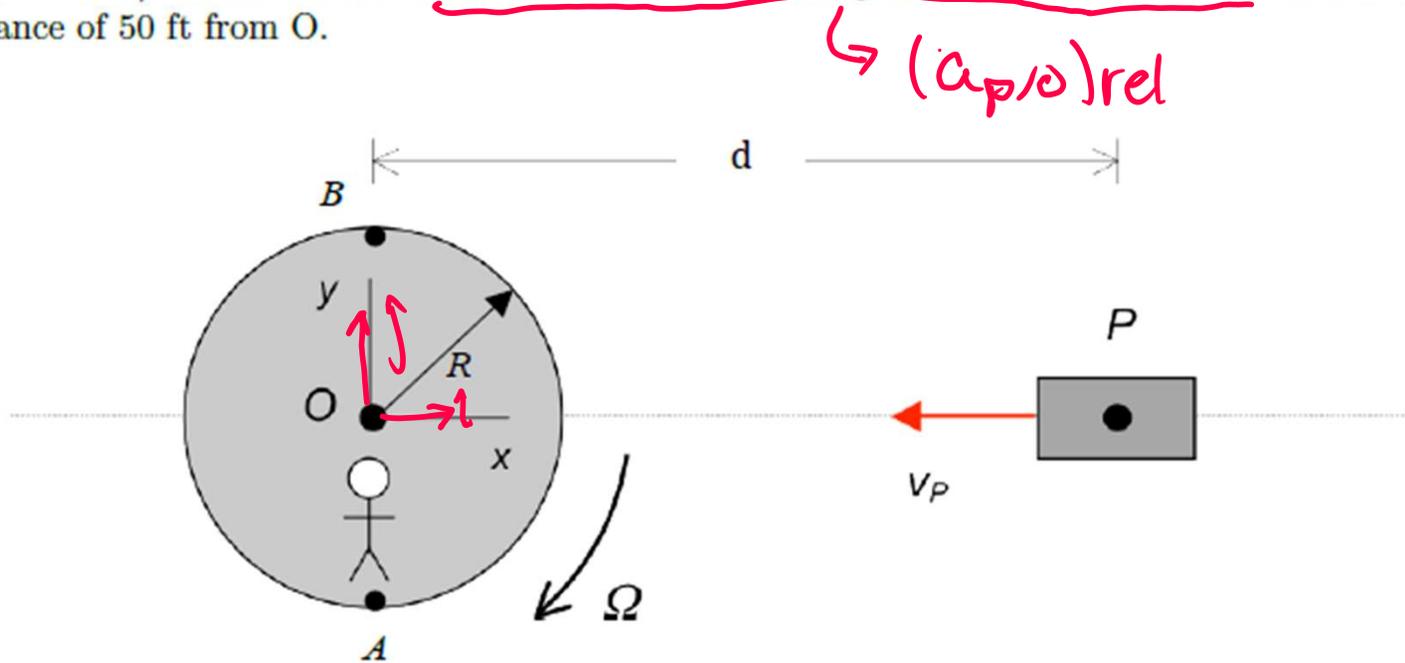
$$(\vec{a}_{P/O})_{rel} = -3 \hat{i}$$

$$\hat{i} = \hat{j} \quad \hat{j} = -\hat{i}$$



### Question C3.2

A disk is pinned to ground at its center  $O$  with the disk rotating clockwise at a constant rate of  $\Omega = 3 \text{ rad/s}$ . Block  $P$  is traveling to the left along a straight path toward  $O$  with a constant speed of  $v_P = 20 \text{ ft/s}$ . Determine the acceleration of  $P$  as seen by an observer on the disk when  $P$  is at a distance of 50 ft from  $O$ .



$$\vec{a}_P = \vec{a}_O + (\vec{a}_{P/O})_{rel} + \vec{\alpha} \times \vec{r}_{P/O} + 2\vec{\omega} \times (\vec{v}_{P/O})_{rel} + \vec{\omega} \times [\vec{\omega} \times \vec{r}_{P/O}]$$

$$(\vec{a}_{P/O})_{rel} = \vec{a}_P^0 - \vec{a}_O - \vec{\alpha} \times \vec{r}_{P/O} - 2\vec{\omega} \times (\vec{v}_{P/O})_{rel} - \omega^2 \vec{r}_{P/O}$$

$$= 0 - 0 - 0 + 2\Omega \hat{k} \times (\vec{v}_{P/O})_{rel} - \Omega^2 d \hat{i}$$

$$\vec{v}_P = \vec{v}_O + (\vec{v}_{P/O})_{rel} + \vec{\omega} \times \vec{r}_{P/O}$$

$$\Rightarrow (\vec{v}_{P/O})_{rel} = \vec{v}_P - \vec{v}_O - \vec{\omega} \times \vec{r}_{P/O}$$

$$= -\vec{v}_p \hat{i} + \Omega \hat{k} \times (d\hat{i})$$

$$(\vec{v}_{p/o})_{rel} = -v_p \hat{i} + \Omega d \hat{j}$$

$$(a_{p/o})_{rel} = 2\Omega \hat{k} \times (-v_p \hat{i} + \Omega d \hat{j}) - \Omega^2 d \hat{i}$$

$$= -2\Omega v_p \hat{j} - 2\Omega^2 d \hat{i} - \Omega^2 d \hat{i}$$

$$= -3\Omega^2 d \hat{i} - 2\Omega v_p \hat{j}$$

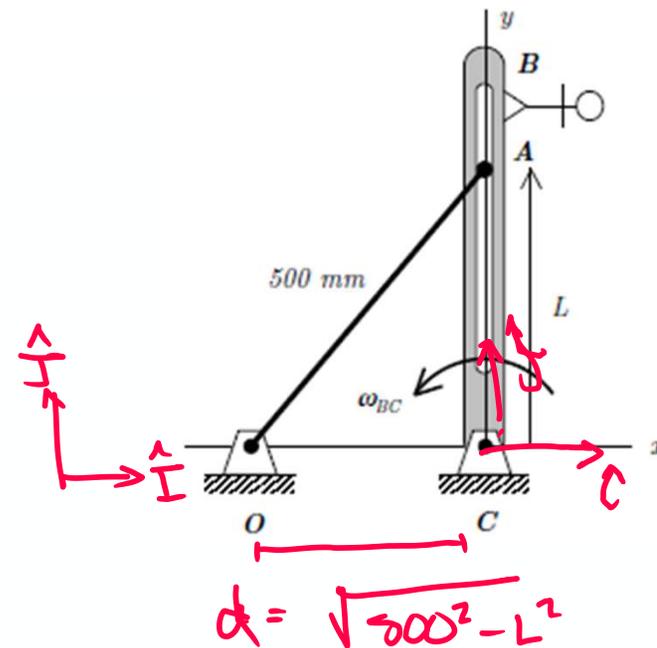
### Example 3.A.5

**Given:** The mechanism shown below is made up of links OA and BC. Links OA and BC are pinned to ground at points O and C, respectively. Pin A of link OA is able to slide within a slot that is cut in link BC, as shown. Pins O and C are on the same horizontal line. Let the  $xyz$  axes be attached to link BC. At the instant shown:

- Link BC is vertical with  $L = 400$  mm; and
- Link BC is rotating counterclockwise at a rate of  $\omega = 6$  rad/s.

**Find:** Determine:

- The angular velocity of link OA at the instant shown; and
- The value for  $\dot{L}$  at the instant shown.



1) Link OA

$$\begin{aligned}\vec{V}_A &= \vec{V}_O + \vec{\omega} \times \vec{r}_{A/O} \\ &= \omega_{OA} \hat{k} \times (d\hat{i} + L\hat{j}) \\ &= \omega_{OA} d\hat{j} - \omega_{OA} L\hat{i}\end{aligned}$$

2) A relative to C

$$\begin{aligned}\vec{V}_A &= \vec{V}_C + (\vec{V}_{A/C})_{rel} + \vec{\omega}_{BC} \times \vec{r}_{A/C} \\ &= \dot{L}\hat{j} + \omega_{BC} \hat{k} \times L\hat{j}\end{aligned}$$

Set =

$$= L\dot{j} - \omega_{BC} L \hat{i}$$

$$L\dot{\hat{j}} - \omega_{BC} L \hat{\dot{i}} = \omega_{OA} d \dot{j} - \omega_{OA} L \hat{\dot{i}}$$

$$\text{here, } \hat{j} = j \quad \hat{i} = i$$

Split into components

$$\hat{i}: -\omega_{BC} L = -\omega_{OA} L \rightarrow \omega_{BC} = \omega_{OA}$$

$$\hat{j}: L = \omega_{OA} d$$

### Example 3.A.7

**Given:** The disk rolls without slipping to the right with a constant angular speed of  $\omega_d$ . At the instant shown, pin P is directly above the center A of the disk.

**Find:** Determine:

- The angular acceleration of the disk; and
- The acceleration of P as seen by an observer on arm BD.

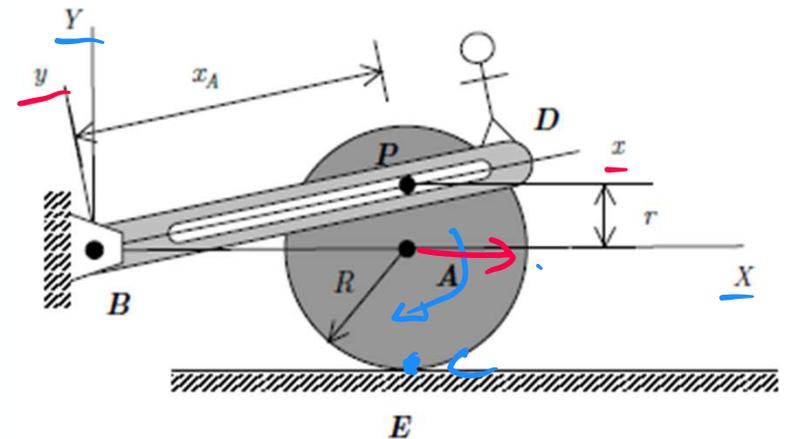
Use the following parameters in your analysis:  $\omega_d = 20$  rad/s (clockwise),  $x_A = 0.48$  m,  $r = 0.14$  m and  $R = 0.2$  m.

velocity of P + P.

$$\begin{aligned}\vec{V}_P &= \vec{V}_C + \vec{\omega} \times \vec{r}_{P/C} \\ &= -\omega_d \hat{k} \times (R-r) \hat{j} \\ &= (R-r)\omega_d \hat{i}\end{aligned}$$

relate P to B

$$\begin{aligned}\vec{V}_P &= \vec{V}_B + (V_{P/B})_{rel} + \vec{\omega}_{BD} \times \vec{r}_{P/B} \\ &= \dot{x}_A \hat{i} + \omega_{BD} \hat{k} \times x_A \hat{i} \\ &= \dot{x}_A \hat{i} + \omega_{BD} x_A \hat{j}\end{aligned}$$



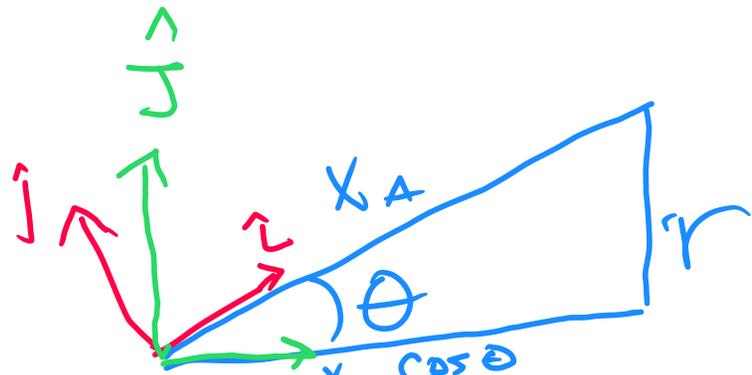
set eqns =

$$(R+r)\omega_d \hat{I} = \dot{x} \hat{I} + \omega_{BD} x_A \hat{J} \quad *$$

write  $\hat{i}, \hat{j}$  in terms of  $\hat{I} \leftrightarrow \hat{J}$

$$\hat{i} = \cos\theta \hat{I} + \sin\theta \hat{J}$$

$$\hat{j} = -\sin\theta \hat{I} + \cos\theta \hat{J}$$



$$\sin\theta = \frac{r}{x_A} \rightarrow \text{find } \theta$$

Sub in to \* & split up components

$$\hat{I}: (R+r)\omega_d = \dot{x} \cos\theta - \omega_{BD} x_A \sin\theta$$

$$\hat{J}: 0 = \dot{x} \sin\theta + \omega_{BD} x_A \cos\theta$$

Solve for  $\dot{x}$  &  $\omega_{BD}$

acceleration of pt P

$$\vec{a}_P = \vec{a}_A + \vec{\omega}_A \times \vec{r}_{P/A} - \omega_A^2 \vec{r}_{P/A}$$

$$= -\omega_A^2 r \hat{j}$$

$$\vec{v}_A = \vec{0}$$

$$\vec{a}_A = \text{const}$$

$$\vec{\omega}_A = \vec{0}$$

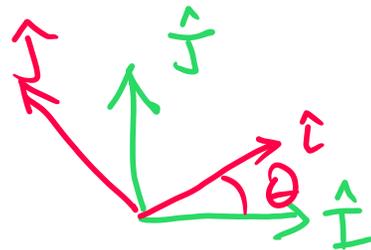
relate acceleration of P + B

$$\vec{a}_P = \vec{a}_B + (a_{P/B})_{rel} = \vec{a}_B + \vec{\omega}_{BD} \times \vec{r}_{P/B} + 2\vec{\omega}_{BD} \times (v_{P/B})_{rel} - \omega_{BD}^2 \vec{r}_{P/B}$$

$$= \vec{0} + \ddot{x}_A \hat{i} + \alpha_{BD} \hat{k} \times x_A \hat{i} + 2\omega_{BD} \hat{k} \times \dot{x}_A \hat{i} - \omega_{BD}^2 x_A \hat{i}$$

$$= \ddot{x}_A \hat{i} + \alpha_{BD} x_A \hat{j} + 2\omega_{BD} \dot{x}_A \hat{j} - \omega_{BD}^2 x_A \hat{i}$$

set  $\vec{a}_P = \vec{a}_P$



$$\hat{j} = \sin\theta \hat{i} + \cos\theta \hat{j}$$

$$-\omega_{BD}^2 r (\sin\theta \hat{i} + \cos\theta \hat{j}) = \ddot{x}_A \hat{i} + \alpha_{BD} x_A \hat{j} + 2\omega_{BD} \dot{x}_A \hat{j} - \omega_{BD}^2 x_A \hat{i}$$

Break into components

$$\hat{\imath} : -\omega_D^2 r \sin\theta = \ddot{x}_A - \omega_{BD}^2 x_A$$

$$\hat{\jmath} : -\omega_D^2 r \cos\theta = \alpha_{BD} x_A + 2\omega_{BD} \dot{x}_A$$

Solve for  $\alpha_{BD}$ ,  $\ddot{x}_A$